HYDROLOGIC IMPACTS OF THE SNOWCREEK GOLF COURSE EXPANSION ON THE AB AND CD HEADWATER SPRINGS

Prepared for

DEMPSEY CONSTRUCTION CORPORATION

September 1996

Mark J. Wildermuth, Water Resources Engineer 415 North El Camino Real Suite A, San Clemente California 92672 714-498-9294

TABLE OF CONTENTS

Section - Description	Page
SECTION 1 INTRODUCTION	1
PURPOSE	1
SCOPE	2
SECTION 2 MAMMOTH BASIN GEOLOGIC AND HYDROLOGIC SETTING	3
STUDY AREA	3
PRECIPITATION AND CLIMATIC VARIABILITY	3
GEOLOGY AND HYDROGEOLOGY OF THE MAMMOTH BASIN AREA	7
Rock Formation Water Bearing Characteristics	11
The Mammoth Basin Groundwater Regime	12
Groundwater Development in the Mammoth Basin	18
Groundwater Storage	20
Surface Water Discharge and Spring Discharge Characterization	22
TEMPERATURE AND WATER QUALITY	33
RELATIONSHIP BETWEEN HISTORICAL GROUNDWATER EXTRACTION AND	37
DISCHARGE AT THE AB AND CD HEADSPRINGS	
SECTION 3 FUTURE WATER DEMANDS AND SUPPLIES	43
CURRENT DEMANDS AND WATER SUPPLY SOURCES	43
FUTURE WATER DEMANDS AND WATER SUPPLY SOURCES	47
FUTURE WATER SUPPLY SCENARIOS	47
SECTION 4 IMPACT OF NEW GROUNDWATER PRODUCTION	55
ON HOT CREEK HEADSPRINGS	
ASSUMPTIONS AND METHODOLOGY	55
IMPACTS ON SPRING DISCHARGE	55
IMPACTS ON SPRING DISCHARGE TEMPERATURE	57
IMPACTS ON SPRING DISCHARGE WATER QUALITY	57
SECTION 5 REFERENCES	62
APPENDIX	
PLATES	

LIST OF TABLES

Table Number	Description	Page
1	PRECIPITATION AND SURFACE DISCHARGE AT MAJOR STATIONS MAMMOTH BASINS	8
2	TOTAL GROUNDWATER USE IN MAMMOTH BASIN AREA	21
3	MONTHLY DISTRIBUTION OF DISCHARGE FOR MAMMOTH CREEK AT OLD 395	25
4	HEADSPRING FLOW IN FISH HATCHERY AREA	26
5	MONTHLY DISTRIBUTION OF DISCHARGE FOR HOT CREEK AT FLUME	27
6	FLOW COMPONENTS FOR HOT CREEK AT FLUME	32
7	WATER QUALITY DATA AT SELECTED STREAM AND SPRING LOCATIONS	34
8	PROJECTED WATER DEMANDS FOR MAMMOTH LAKES AREA	44
	INCLUDING MAMMOTH COMMUNITY WATER DISTRICT AND ADJACENT PRIVATELY SERVED LANDS	
9	MONTHLY WATER DEMAND BY WATER USER GROUP	45
10	WATER PRODUCTION BY MCWD AND SNOWCREEK	46
11	WATER SOURCES AND ALLOCATION FOR MCWD	49
12a	MONTHLY WATER SUPPLY ALLOCATIONS FOR SCENARIO 1A	51
12b	MONTHLY WATER SUPPLY ALLOCATIONS FOR SCENARIO 1B	52
12c	MONTHLY WATER SUPPLY ALLOCATIONS FOR SCENARIO 2A	53
12d	MONTHLY WATER SUPPLY ALLOCATIONS FOR SCENARIO 2B	54
13	PROJECTED WORST-CASE IMPACTS FROM CUMULATIVE AND INCREMENTAL	56
	NEW WATER PRODUCTION MCWD SERVICE AND SURROUNDING AREAS SPRING DISCHARGE	
14	PROJECTED WORST-CASE IMPACTS FROM CUMULATIVE AND INCREMENTAL NEW WATER PRODUCTION MCWD SERVICE AND SURROUNDING AREAS TEMPERATURE	58
15	PROJECTED WORST-CASE IMPACTS FROM CUMULATIVE AND INCREMENTAL NEW WATER PRODUCTION MCWD SERVICE AND SURROUNDING AREAS TOTAL DISSOLVED SOLIDS	59
16	PROJECTED WORST-CASE IMPACTS FROM CUMULATIVE AND INCREMENTAL NEW WATER PRODUCTION MCWD SERVICE AND SURROUNDING AREAS HARDNESS	60
17	PROJECTED WORST-CASE IMPACTS FROM CUMULATIVE AND INCREMENTAL NEW WATER PRODUCTION MCWD SERVICE AND SURROUNDING AREAS TOTAL INORGANIC NITROGEN	61

LIST OF FIGURES

Figure Number	Description	Page
1	MAMMOTH BASIN LOCATION MAP	4
2	MAMMOTH BASIN VICINITY MAP	5
3	MEAN ANNUAL PRECIPITATION	6
	ISOHYETAL MAP OF THE MAMMOTH BASIN	
4	ACCUMULATIVE DEPARTURE FROM MEAN FOR KEY HYDROLOGIC	9
	TIME SERIES IN THE MAMMOTH BASIN	
5	GEOLOGIC MAP OF THE MAMMOTH BASIN	10
6	WATER LEVEL ELEVATIONS ALONG CROSS SECTIONS A-A'-B	14
	EAST-WEST THROUGH MAMMOTH VALLEY GROUNDWATER BASIN	
7	WATERSHED AND SUB-DRAINAGE AREAS OF THE MAMMOTH BASIN	16
8	SPRINGS AND TEST POINTS IN THE VICINITY OF THE HOT CREEK	19
	STATE FISH HATCHERY	
9	OWEN'S VALLEY TUI CHUB HABITAT AT THE AB HEADSPRING	24
10	COMPARISON OF RUNOFF IN MAMMOTH BASIN TO	28
	APRIL 1 SNOW SURVEY	
11	MONTHLY DISTRIBUTION OF SURFACE WATER FLOW	29
12	MONTHLY DISTRIBUTION OF FLOW AT HOT CREEK HEADSPRINGS	31
13	DOUBLE MASS CURVE FOR	39
	MAMMOTH CREEK AT OLD 395 AND APRIL 1 SNOW SURVEY	
14	DOUBLE MASS CURVE FOR	40
	HOT CREEK AT THE FLUME AND APRIL 1 SNOW SURVEY	

SECTION 1 INTRODUCTION

PURPOSE

The purpose of this study is to estimate the impacts, if any, of present and future groundwater extraction in the Mammoth Basin area on the AB and CD headsprings near the Hot Creek Fish hatchery. The AB and CD spring discharge channels are habitats for the endangered Owens Valley tui chub (Gila bicolor snyderi). The biologic assessment of spring flow impacts will be done by others and is not included in this report. The specific impacts that are to be investigated include:

"the effect of groundwater pumping on spring flows at the AB and CD headsprings. For the analysis, spring flows include the discharge, timing of discharge and water quality parameters." (July 1, 1996 letter from Dennis Martin, United States Department of Agriculture, Forestry Service to Diane Noda, Fish and Wildlife Service).

This analysis will examine the direct, indirect and cumulative effects of the Snowcreek golf course and current extractions by the Mammoth Community Water District (MCWD) and will include:

"Determination of golf course groundwater extraction and timing.

Determination of Water District extraction and timing

Characterization of Mammoth Creek surface flows focusing on volume and timing.

Characterization of the flows at the AB and CD headsprings, including flow volume, timing and water quality parameters" (July 1, 1996 letter from Dennis Martin, United States Department of Agriculture, Forestry Service to Diane Noda, Fish and Wildlife Service).

This report describes the hydrologic impacts of the proposed Snowcreek golf course expansion. Expansion of the Snowcreek golf course will require an increase in irrigation supply to the golf course that in turn may require: an increase in groundwater extraction, use of reclaimed water, or

both. The California Department of Fish and Game and the U. S. Fish and Wildlife Service have expressed concern regarding potential changes in spring flow at the AB and CD headsprings that could be caused by future increases in groundwater extraction that may be caused specifically by expansion of the Snowcreek golf course, and in general by expanded urban and recreational land uses in the Mammoth Basin area.

MCWD is the principal water purveyor and wastewater treatment entity in the Mammoth Basin area. MCWD has developed a water supply plan to meet all future water demands using a combination of local water resources, reclaimed water and imported water. This plan includes potential for long term increases in groundwater extraction, some of which could be used for irrigation at the proposed expansion of the Snowcreek golf course (MCWD,1996).

SCOPE

The scope described herein was developed to evaluate the potential hydrologic impacts described above. The scope includes the following tasks:

- Task 1 Collect, compile and review reports and data.
- Task 2 Conduct assessments of the available reports and data to: characterize surface water discharges in the AB and CD headsprings and Mammoth Creek; and to develop relationships, if possible, of historical groundwater extraction in the Mammoth Basin and discharge at the AB and CD headsprings.
- Task 3 Describe future and ultimate water demands in the Mammoth Basin.
- Task 4 Describe impacts, if any, of increased groundwater extraction from the proposed expansion of the Snowcreek golf course and for ultimate development, on the AB and CD headsprings.

SECTION 2 MAMMOTH BASIN GEOLOGIC AND HYDROLOGIC SETTING

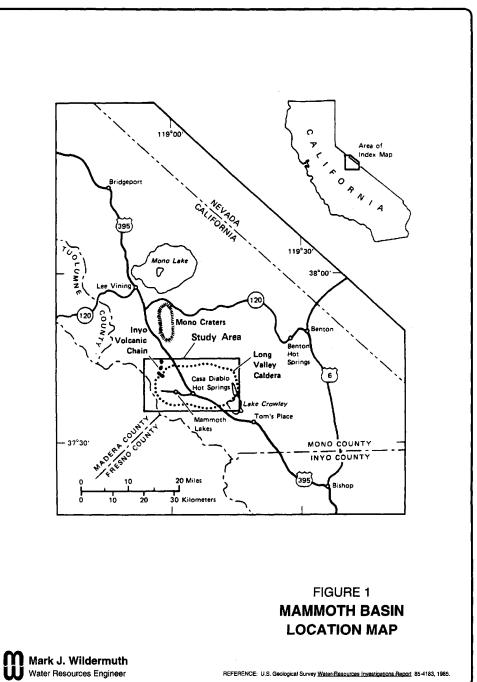
STUDY AREA

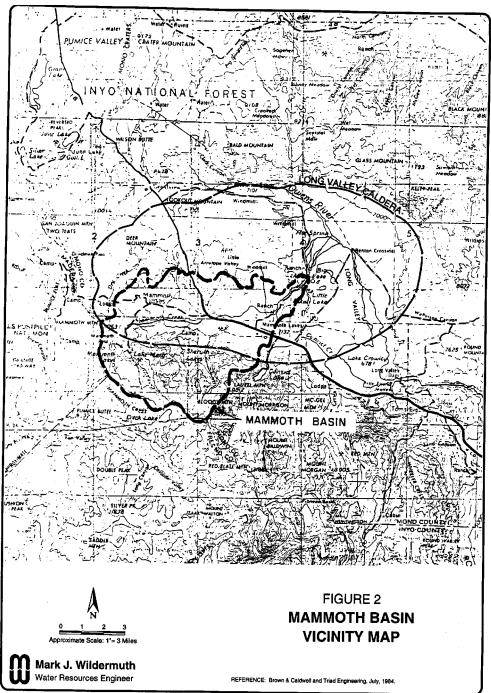
The general study area, shown in Figure 1, is located on the eastern flank of the Sierra Nevada mountain range approximately 30 miles north of the community of Bishop and almost directly west of Lake Crowley. The study area encompasses a total area of about 175 square miles, of which 155 square miles lay within and forms the Long Valley Caldera and some 20 square miles that are south and outside the caldera boundary (see Figure 2). Of primary interest to this study is the watershed area of the Mammoth Creek and Hot Creek which extends 13 miles eastward from Mammoth Mountain to a surface flow gaging station on lower Hot Creek. This area is shown in Figure 2. The topographically defined area of the Mammoth Basin is about 71 square miles and has maximum west-east and north-south dimensions of 13 and 9 miles respectively. Plate 1 shows the locations of wells, springs and other important features

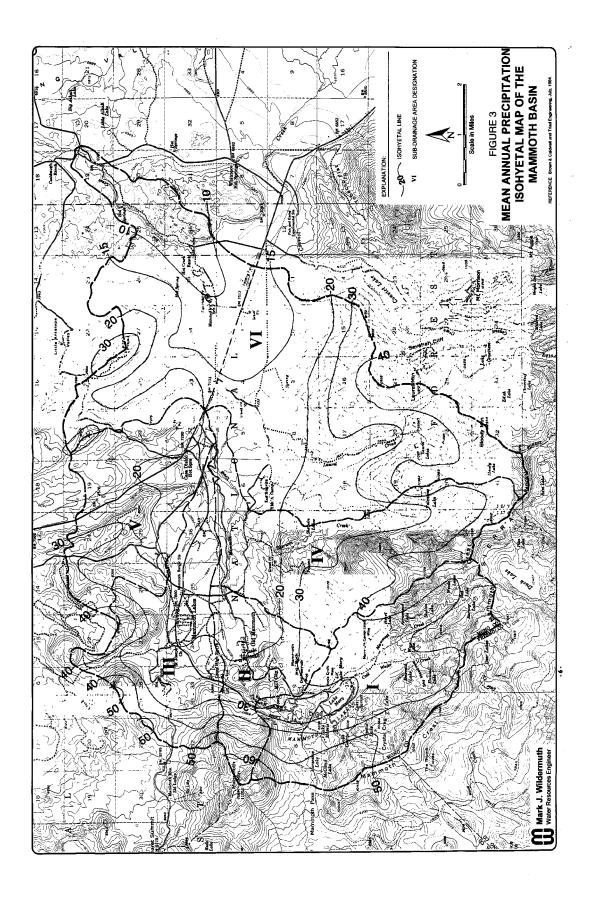
The Mammoth Basin occupies a topographically diverse area on the eastern flank of the Sierra Nevada Mountain Range. Surface elevations range from about 12,500 ft-msl at Bloody Mountain in the southern part of the Basin to about 6,900 ft-msl at the far eastern extreme of the Basin. Surface topography ranges from flat to undulating in the Mammoth valley to sharp and craggy in the western mountainous elevations. The topography may be characterized as an alpine glaciated surface superimposed with extrusive volcanic terrain.

PRECIPITATION AND CLIMATIC VARIABILITY

Studies by the California Department of Water Resources (DWR, 1973) indicated that about 85 percent of all precipitation in the study area occurs during the period of October 1 through April 1. Figure 3 is an isohyetal map of average annual precipitation for the Mammoth Basin developed by DWR (DWR, 1973). Average annual precipitation ranges from about 60 inches in the







western mountainous area to about 10 inches in the extreme eastern part of the Basin. Precipitation occurs as snow and rain. Table 1 lists the annual precipitation totals at the Lake Mary Store station and the water content from the April 1 snow course survey. The Lake Mary Store precipitation data and April 1 snow survey data are collected by the Los Angeles Department of Water and Power (LADWP). Precipitation records at Lake Mary Store started in 1948 and runs to the present. Annual precipitation at Lake Mary Store averages about 28 inches per year and ranges from a high of about 56 inches per year to a low of about 17 inches per year. April 1 snow survey records start in 1943. Snow water content from the April 1 snow surveys average about 43 inches per year and range from a high of about 89 inches per year to a low of about 9 inches per year.

Figure 4 is a plot of the accumulated departure from the mean for precipitation at Lake Mary Store and the April 1 snow survey. The accumulated departure from the mean (ADFM) plot is useful in characterizing wet and dry climatic periods. Negative sloped line segments indicate periods of below mean precipitation, and positively sloped line segments indicate period of above normal precipitation. For example, the period from 1978 to 1986 was a wet period and the period from 1987 to 1992 was a dry period. Review of the entire record for Lake Mary Store and the April 1 snow surveys indicate that the 1978 to 1986 period was the wettest period in the 50-year precipitation record; and that the following dry period of 1987 to 1992 was the most severe drought of record. In fact, applying the ADFM approach to the LADWP/USGS stream flow history for Mammoth Creek at Old 395 indicates that the 1978 to 1986 period was the wettest period in the last 63 years; and that the dry period of 1987 to 1992 was the most severe drought period (in terms of magnitude and length) in the last 63 years. Stream discharge data will be characterized later in this section.

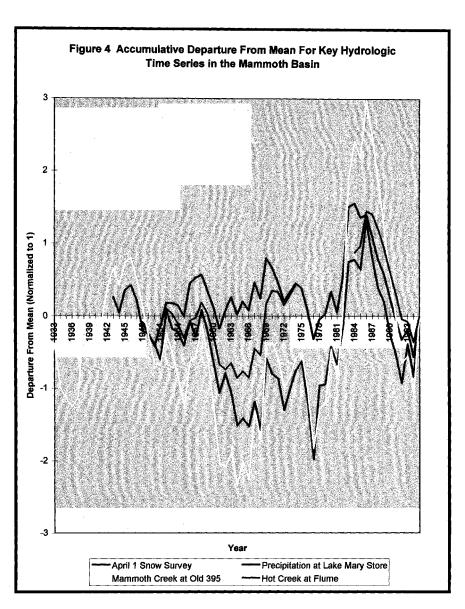
GEOLOGY AND HYDROGEOLOGY OF THE MAMMOTH BASIN AREA

The Mammoth Basin watershed straddles the southern boundary of the Long Valley Caldera. Figure 5 depicts the general surface geology in the project area. Approximately one half of the basin lies inside the downdropped caldera feature and one half is south of and outside the caldera. Mammoth Basin is generally formed by elevated areas on the north and west that are comprised largely of Tertiary extrusive igneous rocks; a central trough filled with Quaternary alluvial and

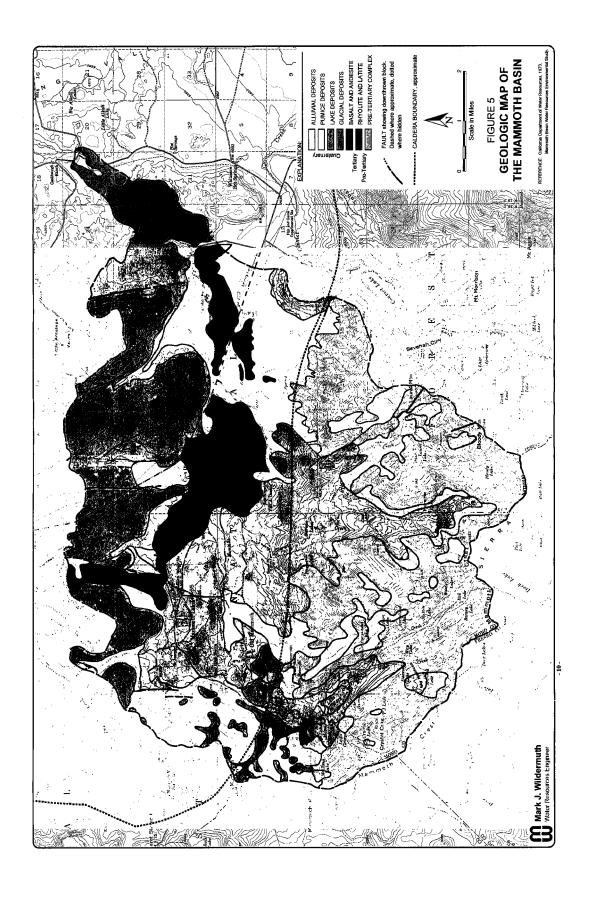
Table 1
Precipistion and Surface Discharge at Major Stations
Mammoth Basins

Year	Apr 1 Snow Surveys (inches/yr)	Precip at Lake Mary Stores (inches/yr)	Mammoth Creek at Old 395 (acre-8/yr)	Hot Creek at Flume (ecre-flyr)
1933			9.860	
1934			6,136	
1935 1936			13,650 14,125	
1937			18,069	
1938			32,544 10,193	
1940			15,628	
1941			21,655	
1942 1943	54.70		23,873 19,990	
1944	34.30		12,314	
1945	57.30		20,914	
1946 1947	48.20 34.50		16,806 11,210	
1948	25.30	25.93	9,982	
1949	41.30	23.54	9,481	
1950 1951	37.90 33.60	24.05 36.44	9,812 15,741	36,915
1952	73.70	37.50	22,986	51,491
1953	32.30	28.35	11,574	38,958
1964 1965	41.60	27.60	10,449	36,180
1955	35.20 58.40	24.12 41.50	9,581 25,935	33,860 52,246
1957	34.20	30.75	18,411	43,655
1958	59.50	29.65	23,128	50,971
1959 1960	30.80 24.30	22.00 22.06	8,261 5,264	35,454 29,221
1961	25.60	20.00	3,487	25,437
1962	55.40	35.65	15,358	39,080
1963 1964	31.40 24.20	33.75 21.69	18,965 9,114	45,754 33,53
1965	48.00	33.60	20,877	45,94
1966	38.50	24.90	12,159	38,482
1987 1988	58.50 26.50	39.50 22.25	30,780 9,724	59.016 38,314
1969	86.50	44.30	36,702	72.12
1970	34.10	24.65	16,453	49,65
1971 1972	41.00 24.50	22.65 21.10	12,773 9,034	41,323 34,421
1973	56.10	32.15	18,041	47,74
1974	54.80	31.95	20,823	48,32
1975 1975	49.10 18.80	26.50 19.68	17,468 7,388	
1977	9.20	17.28	3,151	
1978	87.80	36.18	24,617	
1979 1980	44.40 66.30	30.61 37.37	17,248 27,877	
1981	32.70	20.11	9,566	
1982	85.40	42.58	30,091	
1983	83.70 44.70	55.90 29.90	45,812 24,077	60.78
1985	37.70	22.88	12,103	45,83
1986	72.90	29.57	28,699	62,09
1987	21.40 24.90	19.94 19.46	8,110 5,973	40.63 33,50
1989	35.50	22.58	5,845	31,38
1990	24.10	19.30	5,074	27,95
1991	31.10 26.30	20.00 20.40	6,918 5,842	29,31 27,29
1993	67.10	32.60	17,449	40,49
1994 1995	24.00 80.00	17.55 44.60	7,487 33,224	30,10 57,36
Average	43.06	28.44	15,929	42,49
Std. Dev. Coef of Var.	18.33 43%	8.35 29%	8,638 55%	10,96 261
Max	87.80	55.90	45,812	72,12
Min	9.20	17.28	3,151	25,43

accumdop — table 1 9/20/96 ·1.



Basic Statistics - Accum Dep from Mean



glacial debris; and an abrupt southern flank of Pre-Tertiary igneous intrusive and metamorphic rocks. The central trough area opens and drains to the east through Quaternary glacial and alluvial deposits to the Owens River and Lake Crowley. Quaternary lake deposits occur sporadically within the eastern portion of the Basin. Numerous faults occur in the extrusive igneous rocks along the northern flank of the basin, while few faults have been mapped in the central and southern parts of the basin

Rock Formation Water Bearing Characteristics

Previous studies have indicated more than 20 geologic rock units are present in the project area. For hydrogeologic purposes, these rock units can be grouped into five general formation categories. The relative water bearing characteristics of the rock formations exposed and underlying Mammoth Basin are described herein for the rocks from youngest to oldest in age.

Quaternary Alluvial Deposits (Qad) - This formation is comprised of detritus derived from all other rock formations in the project area. Such deposits are comprised of clay, silt, sand, cobbles and boulders that are generally unconsolidated and range in thickness from a thin wedge to an estimated 60 feet (DWR, 1973). These alluvial deposits range in permeability from low to moderate, and do not constitute large groundwater reservoirs because of their limited thickness and areal occurrence.

Quaternary Lake Deposits (Ql) - These lake sediments were deposited during the upper Pleistocene epoch in a large regional lake that was created by the damming of the upper Owens River Valley by volcanic and glacial rock materials. The lake deposits are most frequently comprised of unconsolidated fine grained sediments that are of low permeability and produce only small-to-moderate quantities of water. Depths of these deposits range to over 200 feet regionally. However, in the Mammoth Basin, depths appear to reach only to a few tens of feet in localized areas and therefore do not appear to constitute significant aquifers.

Quaternary Glacial Deposits (Qg) - During the Quaternary (Pleistocene) epoch, alpine glaciation was active throughout a large area of the Sierra Nevada Ranges. Remnants of this glaciation continue to persist today in some of the higher mountainous elevations. Within the project area,

features related to glaciation and glacial deposition are present, for the most part, in the southern and central sectors of Mammoth Basin. The glacial deposits are slightly to moderately consolidated, consist of clay to boulder size fragments and provide locally good groundwater sources and storage. Such materials were deposited at several glacial and inter-glacial intervals throughout the Pleistocene epoch and vary in thickness from a few feet to more than 100 feet.

Quaternary through Tertiary Igneous Rocks (Vb), (Vr) - These rock formations consist of lava flows, breccias and tuffs inter-bedded with glacial debris. Types of rock include basalt, rhyolite, latite and andesite. These formations occur mainly in the northern and western parts of the basin and largely within the southern part of the Long Valley Caldera. Secondary porosity in these volcanic rocks along with the inter-bedded glacial sediments produce significant aquifers in the central part of the Mammoth Basin. These rocks range in depth to more than 3,000 feet.

Pre-Tertiary Rocks (pT) - This complex of rocks includes Paleozoic Metasediments, Mesozoic Metavolcanics and Cretaceous intrusive rocks. The rocks contained within this complex include a wide variety of igneous and metamorphic types which occur exclusively in the southern part of the Mammoth Basin. Groundwater in the pre-tertiary rocks is generally associated with the secondary porosity of faults, joint systems and crush and fracture zones. The quantity of groundwater yielded from these rocks in the Mammoth Basin vicinity is usually small. The Pre-Tertiary rocks are the basement complex of the Sierra Nevada.

The Mammoth Basin Groundwater Regime

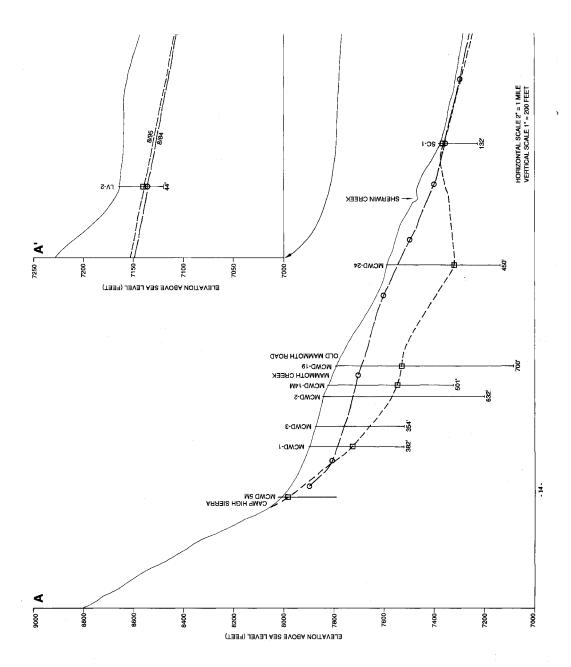
Underlying the Mammoth Basin is a groundwater regime that does not correspond to the boundaries of the surface drainage systems. Previous studies in the project vicinity have implied that the Mammoth Basin groundwater regime is a part of the Long Valley Caldera groundwater system. It is doubtful, however, that a single system prevails throughout the caldera and/or the Mammoth Basin considering the complex geology, hydrology and hydrogeology of the area. It also appears from earlier studies that two, and perhaps more, groundwater regimes are present.

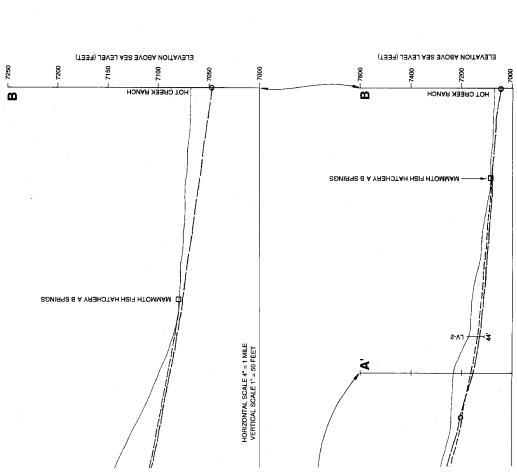
The groundwater basin lies largely within the central part of the Mammoth Basin watershed. Boundaries of the groundwater basin have not been specifically defined due to the complex hydrogeologic conditions of the basin. Nevertheless, a general outline of the basin can be made considering surface drainages, ground elevations, surface geology and earlier subsurface exploration. A generalized outline of the Mammoth-Hot Creek groundwater basin is shown on Plate 1. The basin as shown extends from near Mammoth Mountain Ski Lodge in the west, through the areas of Old Mammoth and Mammoth Lakes, on eastward past the Casa Diablo Hot Springs and the fish hatchery, then continues eastward across the Mammoth Basin boundary into Long Valley. The southern boundary of the Long Valley Caldera appears to closely parallel the southern groundwater basin boundary. The width of the basin varies from about 1.5 to 4.0 miles along its 11 mile east-west course. This area is about 28 square miles. Both surface and groundwater enter the groundwater basin area from the north, west and south. Gradients of surface flows follow stream course elevations, while groundwater gradients are a function of saturated basin cross section, hydraulic conductivity of the rocks, and the rate groundwater is passing through the basin

Figure 6 shows two cross sections (A-B and A'-B;) that pass through a part of Mammoth groundwater basin. The locations of these cross sections are shown on Plate 1. Cross section A-B originates approximately 1 mile west of Camp High Sierra and extends eastward about 9.5 miles to the Hot Creek Ranch. Cross Section A'-B is an expanded scale of a part of section A-B that starts 0.35 mile west of well LV-2 and extends eastward to Hot Creek Ranch. Both sections indicate the ground surface configuration as determined from published topographic maps and recorded elevations of well heads. Extraction and monitoring wells are shown in their relative locations along the section lines. Two water level profiles are plotted:

- Summer 1984, taken from interpretations of estimated water level contours by the USGS in Water Resources Investigation 85-4183 (USGS, 1985).
- Summer 1995, data from records of the USGS and MCWD.

Groundwater level and well construction data were obtained from MCWD and the USGS. The summer 1984 profile is partly from actual water level data and partly from the USGS generalized interpretations that produced a regional water level map (USGS, 1985). The USGS 1984 groundwater levels in the western basin sector are a composite of unconfined, partially confined and confined aquifers. A gap in data occurs in the vicinity of MCWD-24 where a major difference of





USGS and MCWD Data- 1995 (8/95)

O USGS Data- 1984

EXPLANATION:

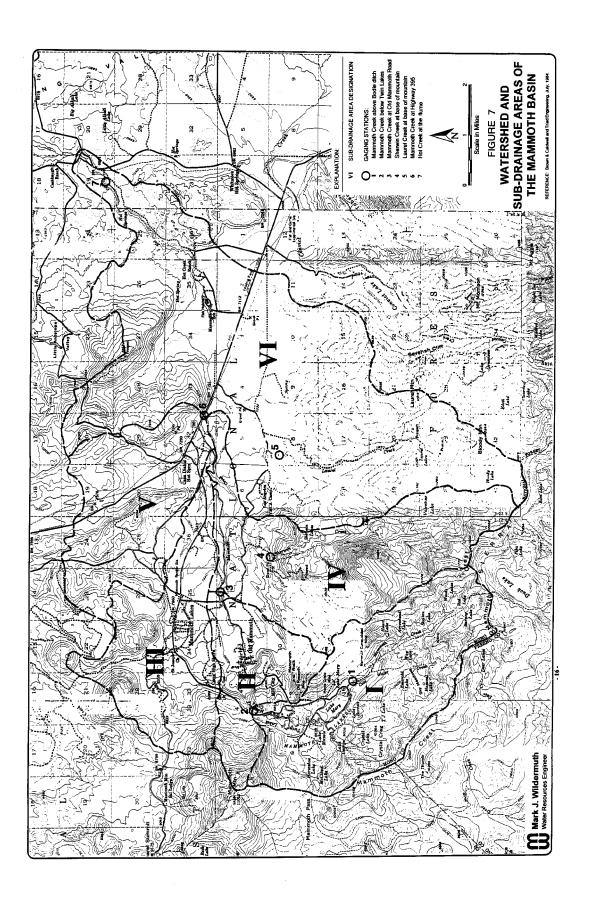
FIGURE 6 WATER LEVEL ELEVATIONS ALONG CROSS SECTIONS A-A-B EAST-WEST THROUGH MAMMOTH VALLEY GROUNDWATER BASIN

water levels can be noted. Such levels were interpreted to be between 7,500 and 7,600 feet in 1984 by he USGS, while an actual measurement in 1995 at MWD-24 had a static level of about 7,330 feet It is probable that errors in the interpretations of water levels for 1984 made by the USGS account, at least partially, for the water level differences observed in Figure 6 between summer 1984 and summer 1995. Another possibility is that the 1984 water levels represent those of a shallow unconfined aquifer while those of 1995 are represent deeper confined and semi-confined aquifers. The latter condition appears to be confirmed by 1990 through 1996 water level measurements that rise and fall seasonally and annually within a relatively narrow range, as shown in the groundwater level hydrographs on Plate 2.

DWR divided the Mammoth groundwater basin into eastern and western areas. The dividing point used by DWR is located near the Los Angeles YMCA Camp along the northern boundary of Section 7, T4S/R28E. Figure 7 is a surface water drainage map of the Mammoth Basin (Brown and Caldwell - Triad Engineering, 1994). For purposes of this investigation, the Basin was divided into eastern and western areas -- the dividing line across the groundwater basin being the eastern boundary of sub-drainage areas IV and V of the Mammoth Basin. This subdivision of drainage occurs at the location of the Mammoth Creek at Old 395 stream gage. The eastern drainage boundary of sub-drainage areas IV and V divides the Mammoth-Hot Creek Groundwater Basin into areas designated herein as Basin West and Basin East.

Basin West - Basin West receives surface drainage from sub-drainage areas I, II, III, IV and V which includes about 34.5 square miles. Of that total acreage, approximately 14.4 square miles are included within the groundwater basin in Basin West. Numerous extraction and monitoring wells have been constructed in Basin West, primarily by MCWD. These wells have drilled to depths of more than 700 feet. Geothermal groundwater is extracted and re-injected in the vicinity of Casa Diablo Hot. The operations of the Casa Diablo facilities are in the extreme eastern part of Basin West and probably outside the hydraulic influence of the MCWD wells that are located about three miles west of the Casa Diablo facilities.

Lithologic logs of wells indicate that inter-bedded alluvium, glacial till and various types of extrusive volcanic rocks comprise the Basin West aquifers. Basin West aquifers appear, from



pumping responses and other data to be confined, semi-confined and unconfined water bearing zones to at least the total depth to which wells have been drilled. Essentially all well extraction in *Basin West* is by MCWD.

The highly variable nature of the subsurface lithology, complex stratigraphic and structural conditions result in a complex aquifer system. Groundwater recharge to the basin is derived from direct percolation of precipitation, and infiltration along Mammoth Creek and other minor streams tributary to the basin. This part of the groundwater basin can potentially receive substantial subsurface recharge because of its western location where basin precipitation is greatest. The location of MCWD wells is shown in Plate 1. Plate 2 contains groundwater elevation time histories (hydrographs) for MCWD extraction wells (shown in pink) located in Basin West. The response of the groundwater levels in these wells indicate that groundwater levels recover almost completely each year, even during periods of lower than normal precipitation.

Outflow to the east from the *Basin West* is by surface outflow and subsurface flow through the eastern boundary of sub-drainage areas III, IV and V into sub-drainage area VI.

Basin East - Basin East is in the surface watershed of sub-drainage area VI and receives surface inflow from sub-drainage III, IV and V via Mammoth Creek. Exclusive of the Mammoth Creek inflow, all surface flows are derived from sub-drainage area VI which includes 33.8 square miles.

The most significant inflowing stream to the Basin East drainage, with the exception of Mammoth Creek, is Laurel Creek which issues from the southern flank of sub-drainage VI. Laurel Creek has a mountainous tributary area of some 5.3 square miles. After leaving the mountain slopes the stream finds its way across the Mammoth valley floor to Mammoth Creek during times of high runoff. During moderate and low flow periods the stream disappears into the alluvial deposits that mantle the valley surface. A number of other streams also enter the valley primarily from springs on the flanking slopes that seasonally cause marshes to form on the surface flats of the basin.

Several extraction wells and test wells have been constructed within *Basin East*. Boring logs for these wells indicate that the subsurface lithology is similar to that found in *Basin West*, i.e., inter-

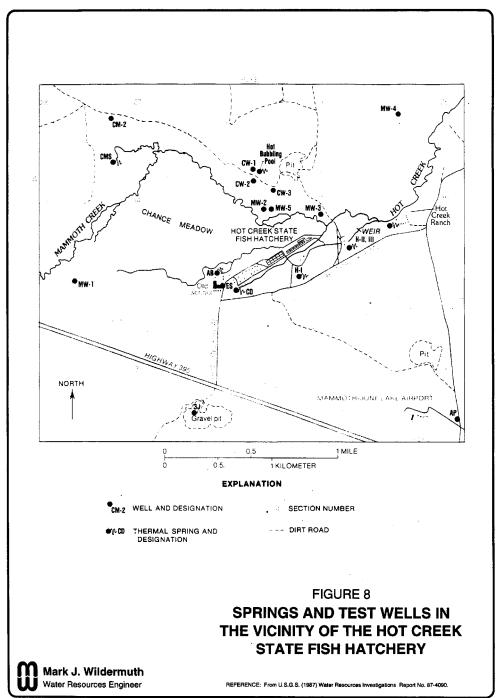
bedded alluvium, glacial till and volcanic extrusives and agglomerates. The Hot Creek headsprings and geothermal waters occur in *Basin East*. The aquifers in the *Basin East* groundwater basin are as complex, or more so, than those in *Basin West*; since they are unconfined, semi-confined and confined, as well as having hot and cold water components.

Recharge in Basin East is derived from direct percolation of precipitation, infiltration along stream courses and subsurface inflows from the south, west and north. The seasonal presence of marshes and shallow groundwater over a large area of the valley surface suggests that this basin, under normal conditions, is refilled completely in most years. The USGS has several monitoring wells in Basin East, the locations of which are shown in Plate 1. Groundwater level hydrographs for wells in Basin East are shown in Plate 2 (green hydrographs). Groundwater levels in Basin East change vary slightly over time in response to climatic variability.

A number of hot springs issue from the surface in sub-drainage area VI. Most significant to this project are those springs in the vicinity of the Hot Creek Fish Hatchery which are designated AB, CD, H1, H23 (see Figure 8). These springs comprise the headwaters of Hot Creek. The USGS (USGS,1987) conducted a detailed analyses of the springs in *Basin East* of the groundwater basin and continues to collect such data that may be relevant to Long Valley Caldera seismic activity, and hydrologic conditions.

Groundwater Development in the Mammoth Basin

Except for possible activities of Native Americans, development of groundwater in the Mammoth Basin did not commence until the late 1800's. This limited early development included the construction of shallow hand-dug wells and the improvement of cool and hot springs. Many of these springs continue to yield water for various uses. Recent groundwater extraction began in January 1976 with the completion of well No. 1 by the Mammoth County Water District (now Mammoth Community Water District). This well was tested to produce at a rate of 512 gallons per minute (gpm) with a specific capacity of 9.4 gallons per minute per foot of drawdown (gpm/ft). Two other wells, Nos. 2 and 3, constructed in the same year were poor producers and not outfitted with pumps. Wells Nos. 6 and 10 were completed in 1988, penetrating fractured basalts



to depths of about 700 feet. Seven wells have been added to the MCWD system since the construction of well No. 1. The recent groundwater extraction history is listed in Table 2. Groundwater extraction has increased from 48 acre-ft/yr in calendar year 1983 to 1,133 acre-ft/yr in 1995. Groundwater extraction peaked at 2,385 acre-ft/yr in 1992 during the 1987 to 1992 drought. A few private wells also produce from the Mammoth Basin, the most significant of which is the Snowcreek golf course well which produced 165 acre-ft in 1995.

Groundwater Storage

The DWR estimated the available groundwater storage in the Mammoth groundwater basin to be about 57,000 acre-ft (DWR, 1973). This estimate is based on useful groundwater occurred only in unconsolidated sediments, specific yield range of 7 to 10 percent, and groundwater level data from only a few wells. Since the DWR completed it study, MCWD has constructed several successful extraction wells into the fractured basalts that underlie the unconsolidated sediments. Useful groundwater storage extends to the basalts that underlie the unconsolidated sediments. For this study, we estimated the useful groundwater storage tributary to the AB and CD headsprings. Useful groundwater storage tributary to the AB and CD headsprings is defined herein as the groundwater in storage that could flow by gravity to AB and CD headwater springs and consists of all drain-able groundwater up-gradient of the headwater springs. The Mammoth Basin up-gradient of the AB and CD headsprings is about 65.9 square miles. For storage analysis, this area can be divided into three areas:

- Mammoth valley area from the fish hatchery westward about 7 miles and averaging about 1.5 miles wide:
- the area defined as the difference between the Mammoth groundwater basin as shown in Plate 1, and the Mammoth valley area described above; and
- the area defined by the difference between the Mammoth Basin drainage area upgradient of the AB and CD headsprings, and the Mammoth groundwater basin.

The Mammoth valley area is about 10.5 square miles. The aquifer in this area consists of relatively thin deposits of alluvium and glacial debris underlain by layers of various types of volcanic rocks to depths of more than 700 feet in the western part of the Mammoth valley area. The surface

Table 2 Total Groundwater Use in Mammoth Basin Area

Years	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Tota
1983	3	0	4	0	0	6	28	2	1	0	0		48
1984	7	٥	11	0	11	22	55	5	19	0	2	25	157
1985	22	6	20	13	36	26	39	82	38	18	13	22	313
1986	14	11	10	3	18	30	42	66	10	0	28	32	264
1987	40	28	40	41	44	68	79	70	57	23	27	47	563
1988	47	54	58	24	40	58	49	51	54	29	59	72	595
1989	88	71	83	6	9	24	193	169	138	46	57	73	958
1990	51	56	38	72	43	118	141	160	192	96	71	84	1,142
1991	171	132	0	98	95	47	120	180	178	99	163	80	1,364
1992	80	121	111	147	76	160	297	413	309	261	158	251	2,385
1993	191	232	115	131	89	224	240	238	182	46	1	24	1,714
1994	76	30	83	65	90	124	244	317	198	51	35	100	1,412
1995	114	99	108	101	61	58	140	239	132	18	12	50	1,133
1996	37	39	34	14	32								
Average	67	63	51	51	46	74	128	153	116	53	48	66	918
Max	191	232	115	147	96	224	297	413	309	261	163	251	2,385
Min	3	0	0	0	0	6	26	2	1	0	0	6	48
% of Annual	7.3%	6.8%	5.6%	5.6%	5.0%	8.1%	14.0%	16.7%	12.6%	5.8%	5.3%	7.2%	100%

Note: includes all pumpage from wells for pump testing, golf course water, and for use by community.

elevation at the fish hatchery springs is about 7,075 ft-msl. From review of Figure 6, the average saturated thickness in this area is about 250 feet. The specific yield of the aquifer materials in this area is estimated to be about 6 percent. The useful groundwater in storage in this area is about 100,800 acre-ft. The remaining part of the groundwater basin area is irregular in shape and does not lend itself to the analysis described above due to a lack of lithologic data and groundwater level data. The area of the remaining part of the groundwater basin area is about 9.5 square miles. Assuming an average saturated thickness of 100 feet and a specific yield of 4 percent the useful groundwater storage in this area is estimated to be about 24,300 acre-ft. The total useful storage in the Mammoth groundwater basin is about 135,100.

The Mammoth Basin drainage area outside the Mammoth groundwater basin is about 45.9 square miles and consists of fractured rock. Assuming an average saturated thickness of 200 feet and specific yield of 2 percent, the useful storage is estimated to be about 117,500 acre-ft. The total useful groundwater storage tributary to the AB and CD headsprings is estimated to be about 242,600 acre-ft.

Surface Water Discharge and Spring Discharge Characterization

Mammoth Creek drains the western part of the Mammoth Basin flowing in a generally easterly direction past Highway 395. Mammoth Creek changes its name to Hot Creek near the Hot Creek Fish Hatchery. Hot Creek leaves the Basin near Cashbaugh Ranch at the eastern end of the Basin and continues about three miles to the northeast to a confluence with the Owens River. Surface flows have been measured at seven gaging stations within the Basin. These stations are listed below.

Station Name	Drainage Area (square miles)
Mammoth Creek above Bodle Ditch	2.8
Mammoth Creek below Twin Lakes	8.3
Laurel Creek at base of mountain	5.6
Sherwin Creek at base of mountain	4.7
Mammoth Creek at Old Highway 395	34.5
Hot Creek at the Flume	68.3

The locations of these stations are shown in Figure 7. Mammoth Creek at Old 395 and Hot Creek at the Flume are long period stations with daily flow records of 40 years or longer. The USGS and others have measured spring discharge from AB, CD and H23 springs since about 1985. The location of the AB and CD headsprings and Owens Valley Tui Chub habitat are shown in Figure 9. Table 3 lists the monthly and annual discharges for Mammoth Creek at Old 395 for the period 1951 through mid 1996; Table 4 lists the monthly and annual discharges for AB, CD, H23 springs for the period of about 1985 through mid 1996; Table 5 lists the monthly and annual discharges for Hot Creek at the Flume for the period 1951 through mid 1996.

Figure 10 shows the average monthly distribution of discharge for Mammoth Creek at Old 395 and for Hot Creek at the Flume. Discharge in Mammoth Creek upstream of the AB, CD and H23 headsprings is seasonal with just over 70 percent of the annual flow occurring in the period May through August. Most of the discharge during this period comes from snow melt. Average annual discharge for the Mammoth Creek at Old 395 averages about 16,000 acre-ft/yr and has ranged from a low of about 3,000 acre-ft/yr to a high of about 46,000 acre-ft/yr.

Downstream at the Hot Creek at the Flume gaging station, about 46 percent of the annual discharge occurs during the May to August snow melt period. In contrast to the upstream Mammoth Creek at Old 395 gaging station, Hot Creek has a significant base flow component fed in part by discharges from the AB, CD and H23 headsprings. Average annual discharge for the Hot Creek at the Flume averages about 42,000 acre-ft/yr and has ranged from a low of about 25,000 acre-ft/yr to a high of about 72,000 acre-ft/yr.

Figure 11 is a graphical comparison of the equivalent water depth from the April 1 snow surveys and the annual runoff for Mammoth Creek at Old 395 and Hot Creek at Flume. The trend lines for annual discharge versus April 1 snow survey is also plotted in Figure 10. The observed annual discharge for Hot Creek at Flume is more scattered about its trend line than the observed annual discharges for Mammoth Creek at Old 395. The coefficient of determination for Hot Creek at flume trend is 0.65 and 0.79 for Mammoth Creek at Old 395. The coefficient of variation (R²) is the fraction of the variance in discharge that can be explained by the variance in April 1 snow surveys. The difference in the trends is due to Hot Creek having a significant groundwater component that can sustain Hot Creek surface discharges in years with low precipitation.

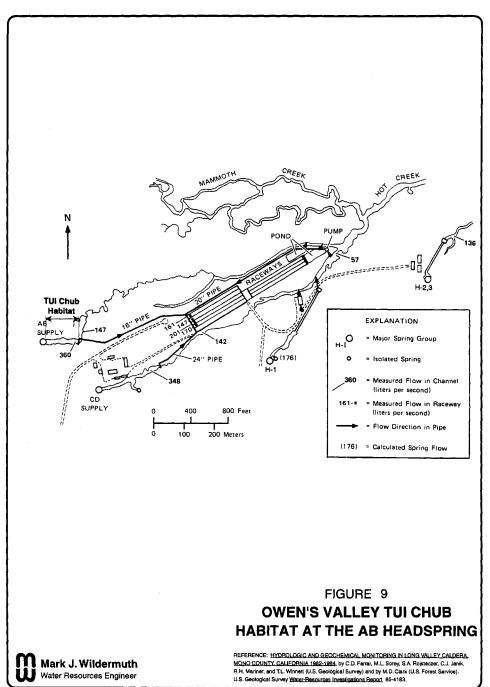


Table 3 Monthly Distribution of Discharge for Mammoth Creek at Old 398

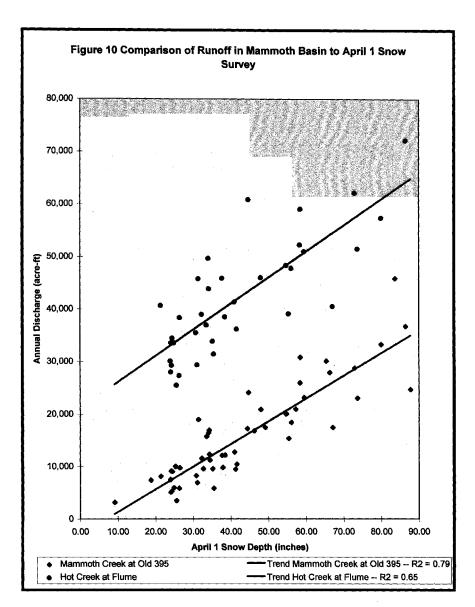
Water Year	Oct	Nov	Dec	Jen	Feb	Mar	Apr	May	nut	Jul	Aug	Sep	To
1960-1951	250	1,880	2,160	770	575	505	743	2.355	3,399	1,854	994	475	15.7
1951-1952	437	340	846	607	480	372	708	3,788	6,158	5,724	2,579	1,147	22,9
1952-1953	748	423	536	651	354	410	821	1,021	2,979	2,725	616	289	11,8
1953-1954	307	295	251	212	278	521	1,068	3,123	2,500	1,221	391	261	10.4
954-1955	144	336	294	323	223	271	497	1,217	4,239	1,355	462	198	9,
955-1958	281	274	1,556	808	448	440	944	3,324	8,526	5,872	2,279	1,186	25,
958-1957	1,024	765	577	565	569	532	700	1,642	6,343	2,471	807	415	16,
957-1958	475	382	389	309	341	439	853	4,662	6,950	4,634	2,419	1,265	23,
958-1959	644	522	429	439	371	502	826	1,447	1,900	586	226	366	8,
959-1960	348	222	241	356	369	412	598	864	1,371	302	95	87	5,
960-1961	136	144	179	188	145	220	192	604	970	332	201	175	3,
961-1962	138	148	227	231	357	349	1,094	2,092	5,548	3,358	1,209	605	15.
962-1963	542	393	426	336	1,048	422	590	2,187	6,232	4,333	1,581	874	18,
963-1964	639	853	636	425	306	471	600	1,492	2,271	723	406	286	9
984-1965	154	347	1,317	937	348	521	836	2,025	5,118	4,438	3,367	1,469	20
965-1966	842	777	587	556	472	586	1,015	3,230	2,321	990	450	345	12,
966-1967	340	303	857	489	475	610	519	3,232	8,411	10,195	3,387	1,983	30
967-1968	1,124	818	592	598	599	531	568	1,640	1,993	753	378	131	
968-1969	232	388	323	277	108	248	962	8,572	11,634	8,806	3,691	1,468	36,
969-1970	1,367	879	697	680	665	779	909	2,548	4,342	2,151	751	485	16
970-1971	453	590	519	425	333	496	593	1,811	4,300	2,099	751	403	12
971-1972	484	516	418	416	298	399	588	1,584	2,768	702	190	664	9
972-1973	519	361	453	430	514	340	518	4,798	6,306	2,314	996	491	18
973-1974	522	1,049	562	593	395	526	801	4,346	7,104	3,006	1,313	606	20
974-1975	516	336	362	368	392	340	477	2,700	7,110	3,118	1,058	694	17
975-1976	1,017	572	460	400	395	466	419	1,805	927	382	326	215	7
976-1977	272	195	127	139	220	225	261	299	904	287	117	107	3,
977-1978	83	77	64	68	46	169	423	3,019	8,894	6,287	2,769	2,719	24
978-1979	1,138	768	457	727	537	606	1,047	4,063	4,388	1,948	947	842	17
979-1980	421	352	312	782	517	463	969	3,770	8,173	7,892	2,918	1,308	27
980-1981	810 393	469 483	372	380 155	392	361 297	648 1.553	2,145	2,679	750	301	259	9
981-1982			414		346			4,978	7,963	6,933	3,447	3,109	30
982-1983 983-1984	2,553 1,813	1,999 1,486	1,318 1,162	857	755 631	782 758	1.093	4,475 4,828	13,277 5,178	11,024 3,496	5,554 1,640	2,551 795	45
	1,813		618	1,218 446	378	343	999	2,722		3,496 988		388	24
984-1985		736		387		967		5,582	2,853		420		12
985-1988 986-1987	362	341 555	413 494	442	392 337	390	1,668 427	1.888	10,659	4,839 549	1,998 262	1,122	28
	1,244												8
987-1968 988-1969	219 188	345 172	276 200	422 271	297 203	306 385	464 589	1,038 1,376	1,306	812 497	302 294	195 253	5
966-1969 989-1990	188 292	1/2 341	218	260	203	385 245	423	1,376 845	1,417 1,065	497 560	294 385	253 214	5
	156	195	112	200 81	96	262	423 259	592	3,050	1,291	480	341	6
990-1991 991-1992	319	401	307	234	226	167	336	1,541	1,046	621	370	275	5
991-1992 992-1993	235	401 272	135	172	198	348	816	3,418	5,555	4,132	1,559	275 810	17
992-1993 993-1994	230 544	445	433	362	350	345	489	1,541	1,828	4,132 548	313	288	7
994-1995	354	326	409	436	394	585	892	2,773	8,224	11,412	5,199	2,220	33
995-1998	1,303	807	821	354	437	399	713	2,784	0,224	11,412	3, 199	2,220	33
Average	600	531	529	451	388	437	718	2,648	4,700	3,096	1,338	764	16
Stan Dev	497	390	404	244	161	167	307	1,608	3,161	3,049	1,371	742	9
oef of Var	83%	73%	76%	54%	47%	38%	43%	61%	67%	98%	102%	97%	- 1
Max	2,553	1,999	2,160	1,218	1,048	967	1,658	8,572	13,277	11,412	5,554	3,109	45
Min	83	77	64	68	46	167	192	299	904	287	95	87	3
of Annual	3.7%	3.3%	3.3%	2.8%	2.4%	2.7%	4.4%	16.4%	29.1%	19.1%	8.3%	4.7%	100

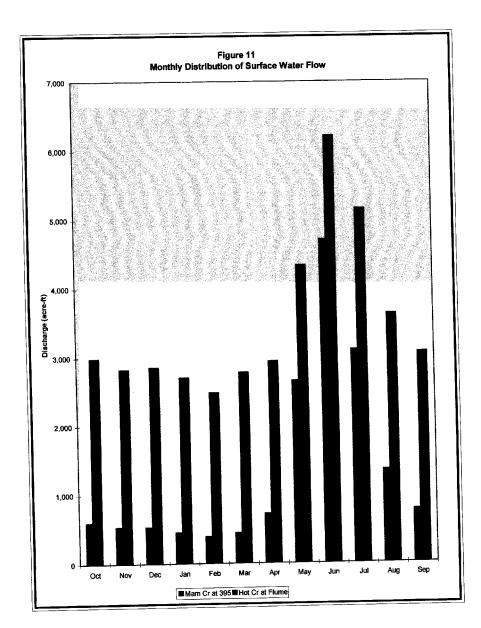
Table 4 Headspring Flow in Fish Hatchery Area

Years	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	То
						AB Sprin	g		············	-	<u> </u>		
1985				516	583	684	700	626	574	552	519	516	
1986	528	470	574	641	715	810	911	829	703	689	580	559	7.9
1987	525	448	497	479	522	531	525	503	442	430	399	393	5.6
1988	374	347	368	350	359	433	436	399	341	400		500	5,0
1989	0.4		444		000	700	700	000	٠.,				
1990													
1991	203	184	209	196	203	344	402	381	301	252	224		
1992	187	163	172	169	196	279	230	193				203	3,1
									178	157	132	132	2,
1993	163	172	178	273	322	463	562	562	473	390	313	264	4,1
1994	233	172	208	175	221	365	344	227	175	166	147	147	2,
1995	175	144	196	322	424	580	789	862	770	632	543	470	5,9
1996	438	393	420	414									
Average	314	277	313	354	394	499	544	509	440	406	357	335	4,
Max	528	470	574	641	715	810	911	862	770	669	580	559	7,
Min	163	144	172	169	196	279	230	193	175	157	132	132	2,
of Annual	6.6%	5.8%	6.8%	7.5%	8.3%	10.5%	11.5%	10.7%	9.3%	8.6%	7.5%	7.1%	10
						CD Sprir	ng .						
1988											424	494	
1989	506	460	508	534	603	503	577	565	470	396	365	479	5.
1990	513	411	537	488	470	482	531	494	473	552	540	525	8.
	485	480				509							
1991			497	454	439		583	651	574	485	439	457	6,
1992	460	433	470	445	448	470	485	460	420	436	399	414	5,
1993	433	405	509	525	519	588	746	660	644	617	485	500	6,
1994	516	448	476	457	466	543	565	519	473	454	362	366	5,
1995	356	316	374	408	491	559	678	675	657	626	549	531	6,
1996	506	457	482	466									
Average	472	424	481	472	477	519	595	575	530	509	445	471	5,
Max	516	460	537	534	519	568	748	675	657	626	549	531	6,
Min	356	316	374	408	439	470	485	480	420	396	362	368	5,
of Annual	7.9%	7.1%	8.1%	7.9%	8.0%	6.7%	10.0%	9.6%	8.9%	8.5%	7.5%	7.9%	10
						H23 Spri	ng						
1987	218	206	224	218	224	224	230	227	215	209	203	203	2,
1988	206	193	215	203	209	208	218	218	196	199	190	193	2,
1989	187	153	178	184	184	187	206	203	190	193	184	184	2,
1990	181	160	181	169	184	184	190	193	203	209	199	208	2,
1991	196	184	184	178	181	181	200	221	187	166	160	169	2,
1992	160	157	166	163	172	181	181	175	153	169	188	172	2.
1993	178	163	184	193	221	230	249	255	233	221	215	190	2.
1994	184	172	196	187	252	242	248	238	233	227	181	190	2,
1995 1996	187 221	169 224	196 227	187 198	193	212	248	249	246	242	215	230	2,
Average	192	178	195	188	202	205	219	220	206	204	190	193	2.
Max	221	224	227	218	252	242	249	255	246	242	215	230	2.
Min	160	153	166	163	172	181	181	175	153	186	160	169	2.
Min of Annual	160 8.0%	7.4%	100 8.2%	7.8%	8.5%	181 8,6%	9,2%	9.2%	8.6%	8.5%	160 8.0%	8.1%	10

Table 6
Monthly Distribution of Discharge for Hot Creek at Flume

Year Water	Oct	Nov	Dec	Jen	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Tot
1950-1951	2.274	3.432	3.912	2,678	2,352	2,411	2,257	3,617	5.190	3,637	2.748	2.437	36.94
1951-1952	2,401	2,177	2,411	2,548	2,228	2.377	3,305	6.623	9,779	8,451	5,267	3,912	51.48
1952-1953	3,448	2.892	2,899	3,030	2,410	2,863	2,877	2,936	4.825	5,493	2,965	2,521	38.9
1953-1954	2,471	2,382	2,307	2.274	2.171	2.764	3.060	4.961	4,724	3,974	2,652	2.407	36,1
1954-1955	2,340	2,276	2,366	2.375	2,110	2.496	2,433	3,167	5,961	3,337	2,673	2,325	33.8
1955-1956	2,327	2.207	3,712	3,219	2,634	2.842	3,290	4.993	9,663	8,606	4.931	3,808	52.2
1956-1957	3,742	3,320	3,111	2,965	2,794	3,001	2,967	3.431	7,770	4,716	3,111	2,913	43.8
1967-1968	2,950	2.752	2,656	2.490	2.380	2.720	3.797	6.732	8,453	7,060	5,019	3,965	50.9
1958-1959	3,400	3,109	2,960	2,905	2,474	3,015	3.021	3,149	3,628	2,727	2,514	2,539	35,4
1959-1960	2,437	2.371	2,437	2,478	2,382	2,533	2,482	2,380	3.025	2,377	2,193	2,146	29.2
1960-1961	2,120	2.050	2,091	2,082	1,980	2,259	2,074	2.173	2,386	2,121	2,021	2,051	25.4
1961-1962	2,173	2,095	2.184	2,166	2,103	2,388	3,576	3,844	7,016	5,371	3,233	2,926	39.0
1962-1963	2,958	2,583	2,585	2,351	3.529	2.675	2,768	4,152	8.312	6.511	3,896	3,428	45,7
1963-1964	3,235	3,185	2,810	2,570	2,354	2,565	2,579	3.021	3,994	2,588	2,379	2.272	33,6
1964-1965	2,309	2,272	2,988	2,824	2,319	2.622	2,868	3,534	7,098	7,172	5,815	4,114	45.9
1965-1966	3.573	3,342	3.097	3.018	2,493	2.972	3,073	4.622	4,200	2,973	2,598	2,503	38,4
1988-1987	2,581	2,397	3,155	2,596	2,434	3,188	3,250	5,108	9,880	12.523	8,643	5,269	50.0
1967-1968	4.282	3,844	3,438	3,263	3.042	2.977	2.835	3.349	3,729	2,791	2,567	2,378	38,2
1968-1969	2,456	2,525	2,500	2,497	2,300	2.890	4,214	11,513	16,151	12,685	7.364	5.018	72,1
1969-1970	4,789	3,863	3,663	3,718	3,260	3,578	3,528	4,686	6.758	5.190	3,456	3,164	49,6
1970-1971	3,148	3,191	3,235	3.085	2,721	2,923	2,681	4,189	6.056	4,300	3,090	2,710	41.3
1971-1972	2,938	2,923	2,685	2,894	2,473	2,786	2,504	3,119	4,586	2.855	2,284	2,797	34,4
1972-1973	2,801	2.619	2,697	2.710	2,511	2,656	3,564	7,173	8.704	5,488	3,669	3,138	47.7
1973-1974	3.059	3,541	3,068	3,095	2,622	2,995	2,944	5.998	8.784	5,390	3,747	3,072	48.3
1974-1975	3,106	2,745	2,709	2,692	2,272	2.658	2,554	0,000	0,700	3,360	3,147	3,012	40,
1983-1984	5,568	5.009	4,811	4,343	3,893	3,899	3,736	6,905	7.644	6,403	4.688	3,795	60.6
1984-1985	4,002	3,930	3,893	3,617	3,126	3,387	3,730	4,910	5,205	3,724	3,207	3,056	45,7
1985-1986	3,002	3,040	3,262	3,306	3,337	4.854	4,962	8.067	10,199	8,275		4,499	
1986-1987	4,561	3,708	3,456	3,282	2.978		2,856				5,610	2,679	62,0 40,5
1967-1968	2,602	2.637	2,703	2.820	2,655	3,294 2,802	2,637	4,008 3,020	3,706	3,155 3,008	2,899		
1967-1966	2,526		2,703						3,441		2,669	2,465	33,4
	2,378	2,542	2,384	2,389	2,271	2,566	2,483 2,185	3,329	3,329	2,625	2,499	2,388	31,3
989-1990		2,346		2,306	2,118	2,417		2,437	2,649	2,358	2,374	2,058	27,9
990-1991	2,015	2,005	1,945	1,969	1,858	2,239	2,384	2,358	4,156	3,099	2,731	2,514	29,
991-1992	2,316	2,237	2,094 1,818	2,086	1,995	2,150	2,106	2,931	2,647	2,473	2,203	2,013	27,2
1992-1993 1993-1994	2,080	1,991		1,963	1,814	2,409	2,967	4,710	7,032	6,476	3,982	3,214	40,4
	2,937	2,600	2,499	2,378	2,102	2,318	2,249	3,072	3,250	2,520	2,191	1,939	30,0
1994-1995 1995-1996	1,955 4,158	1,929 3,42 9	2,090 3,550	2,213 1,622	2,048 1,592	2,731 1,647	3,197 1,811	4,648 1,233	9,487	13,161	8,305	5,515	57,2
Average	2,986	2,824	2,854	2,700	2,477	2,775	2,934	4,327	6,205	5,149	3,616	3,054	42,1
Stan Dev	847	676	641	545	489	519	616	1,967	2,970	3,014	1,567	937	11,1
Coef of Var	28%	24%	22%	20%	20%	19%	21%	45%	48%	50%	43%	31%	2
Max	5,568	5,009	4,811	4,343	3,893	4,654	4,662	11,513	16,151	13,161	8,305	5,516	72,1
Min	1,955	1,929	1,818	1,622	1,592	1,647	1,811	1,233	2,386	2,121	2,021	1,939	25,4
6 of Annual	7.1%	6.7%	6.8%	6.4%	5.9%	8.6%	7.0%	10.3%	14.8%	12.2%	8.6%	7.3%	100.

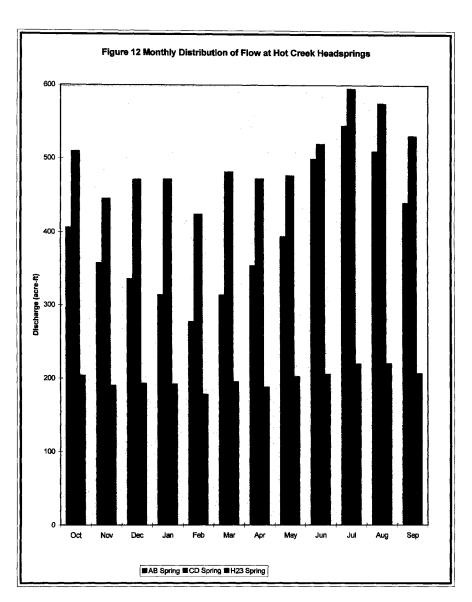




Basic Hydrology -- mon mc hc 10/15/96

Figure 12 shows the monthly distribution of discharge for the AB, CD and H23 headsprings located at the fish hatchery. Daily discharge data for these springs are plotted in Plate 3 for their period of record along with the daily discharge data for Mammoth Creek at Old 395 and Hot Creek at the Flume. Comparable data does not exist for the H1 spring. The AB spring shows a definitive seasonal pattern that consists of two components - a seasonal component that responds rapidly to the magnitude and timing of snow melt runoff (as observed in the Mammoth Creek at Old 395 record; and a more steady base flow component that responds to changes in long term groundwater storage and climatic cycles. Analysis of the daily discharge data for the AB spring and Mammoth Creek indicates that the peak discharge from the AB spring lags behind the Mammoth Creek peak discharge by a period one to two months; and that the AB seasonal component has a recession period of about a five to six months where the Mammoth Creek recession period usually lasts two to three months. This can clearly be seen in Plate 3 by comparing the daily flow hydrograph for the AB headspring and Mammoth Creek at Old 395. In contrast, the CD and H23 springs show only a slight seasonal component with most of the discharge variation coming from changes in long term groundwater storage and climatic cycles. The recorded discharge history for the springs is heavily influenced by the drought of 1987 through 1992 and therefore estimates of average annual discharges based on the available history are probably low. The average annual discharge for the AB, CD and H23 springs for the existing records is 4,700 acre-ft/yr, 6,000 acre-ft/yr and 2,400 acre-ft/yr, respectively.

Table 6 lists the annual discharge of Hot Creek at the Flume, the associated base flow and storm flow components, and the annual flows for the AB, CD and H23 headsprings. The total flow at Hot Creek at the Flume was divided into base flow and storm flow components through a detailed analysis of daily flow data for the period October 1950 to May 1996. Base flow is numerically equal to the total flow minus surface runoff and is comprised of spring flow and other groundwater that discharge to Hot Creek. The base flow estimated for the discharge at the Hot Creek at the Flume gage averages about 27,000 acre-ft/yr and ranges from a low of 16,000 acre-ft/yr to a high of about 42,000 acre-ft/yr. The average fraction of the base flow at the Hot Creek gage contributed by the AB, CD and H23 springs during the 1986 to 1995 period is estimated at 18 percent, 23 percent and 9 percent, respectively.



MCWD Production Data - mon dis ab ed h23 10/15/96

Table 6
Flow Components for Hot Creek at Flume (acre-ft/yr)

	Flow in H	lot Creek at	Flume	Flow	in Springs	
Year	Total	Base	Storm	AB	CD	H23
1950 / 1951	36,943	23,161	13,781			
1951 / 1952	51,403	21,984	29,419			
1952 / 1953	38,948	29,060	9,888			
1953 / 1954	36,168	25,007	11,161			
1954 / 1955	33,859	25,260	8,599			
1955 / 1956	52,153	25,369	26,784			
1956 / 1957	43,840	15,851	27,989			
1957 / 1958	50,963	27,450	23,514			
1958 / 1959	35,443	30,576	4,867			
1959 / 1960	29,136	24,774	4,362			
1960 / 1961	25,407	22,365	3,041			
1961 / 1962	39,072	23,270	15,802			
1962 / 1963	45,749	28,409	17,340			
1963 / 1964	33,411	27,142	6,268			
1964 / 1965	45,933	26,853	19,080			
1965 / 1966	38,472	29,676	8,797			
1966 / 1967	59,003	26,624	32,379			
1967 / 1968	38,141	34,524	3,617			
1968 / 1969	72,114	27,577	44,537			
1969 / 1970	49,653	34,501	15,151			
1970 / 1971	41,308	30,508	10,801			
1971 / 1972	34,331	26,998	7,333			
1972 / 1973	47,732	26,527	21,205			
1973 / 1974	48,315	29,784	18,531			
1983 / 1984	60,495	42,066	18,429			
1984 / 1985	45,879	35,596	10,282			
1985 / 1986	64,501	33,791	30,710	7,988		
1986 / 1987	40.570	36,624	3,946	5,693		2.59
1987 / 1988	33,374	28,409	4,965	5,555		2,44
1988 / 1989	31.341	26,744	4.597		5,865	2.23
1989 / 1990	27,911	24.609	3,302		6,015	2,25
1990 / 1991	29,273	22,632	6,641	3,100	6,033	2,21
1991 / 1992	27,171	22,691	4,480	2,188	5,340	2,01
1992 / 1993	40,437	22,712	17,726	4,134	6,610	2,53
1993 / 1994	30.054	25,405	4.649	2,578	5,647	2,54
1994 / 1995	57,279	21,346	35,933	5,908	6,221	2,57
\verage (acre-ft/yr)	42,105	27,385	14,720	4,513	5,962	2,38
/lin (acre-ft/yr)	25,407	15,851	3,041	2,188	5,340	2,01
/lax (acre-ft/уг)	72,114	42,066	44,537	7,988	6,610	2,59
Coefficient of Variation	27%	19%	73%	47%	7%	99
raction of Total Spring Flow (1986 to 19	195)			18%	23%	99

TEMPERATURE AND WATER QUALITY

Temperature and water quality data for the period of the early to mid 1980' to the present is available for Mammoth Creek at Old 395, the AB headsprings, CD headspring, H23 headspring and Hot Creek at the Flume. These data were collected by the USGS and were obtained from the USGS for this study. These data are summarized in Table 7. A detailed tabular listing of temperature and water quality data for these sites is included in the Appendix. Parameters of interest for the AB and CD headsprings include total dissolved solids (TDS), hardness, total inorganic nitrogen (ammonia plus nitrite plus nitrate expressed as nitrogen), phosphorus (orthophosphate-phosphorus) and arsenic. Temperature, total inorganic nitrogen and phosphorus are parameters of concern for the aquatic habitat. TDS and hardness are general indices of water chemistry. Total inorganic nitrogen and arsenic are human health concerns for the employees of the fish hatchery that use the springs as a domestic supply.

The temperature at the AB spring averages about 16.9 degrees centigrade and ranges from a low of 15.5 degrees centigrade to a high of about 18.0 degrees centigrade. The temperature at the CD spring averages about 15.6 degrees centigrade and ranges from a low of 14.0 degrees centigrade to a high of about 17.0 degrees centigrade. The temperature at the H23 spring averages about 11.3 degrees centigrade and ranges from a low of 10.0 degrees centigrade to a high of about 13.0 degrees centigrade. Plots of discharge versus temperature are included in the appendix for each spring. There is a weak relationship between spring discharge and temperature for the AB spring. Linear regression for temperature as a function of discharge for each spring yielded the following parameters:

Spring	Slope	Intercept	Coefficient of Determination (R2)
AB	-0.1737	17.86	0.4160
$^{\rm CD}$	0.1294	14.50	0.0966
H23	0.2217	10.54	0.0296

The coefficient of determination is the fraction of the variance in temperature that is explained by the variance in discharge. About 40 percent of the variation in temperature in the AB spring can be attributed to variation in AB spring discharge. The temperature variations in the CD and H23 springs are not significantly influenced by variations in discharge at these springs.

Table 7
Water Quality Data
At Selected Stream and Spring Locations
(Data from LIE/28)

Date	ineten.	Water	ρH	EC	TDS			ione					iona			Total	Total
Flow Termp (cits) (°C) (umbo/om) (mg/l)	(mg/l)	Ce (mg/l)	Mg (mg/t)	Na (mgf)	K (mg/l)	(may)	CI (mg/l)	SO4 (mg/l)	MP(M)	(mg/l)	B (mg/l)	Alkalinity (mg/l as C					
						1	0265130	Mammot	h Creek s	# Old 396							
Minimum	1.4	0.5	7.1	42	30	5.1	0.9	2.1	0.6	41	0.1	1.7	0.01	0.10	0.01	28	18
Maximum	76.9	18.0	8.4	165	136	14.0	6.9	13.0	3.0	99	1.2	9.2	0.50	0.30	0.05	86	61
Average	16.2	8.3	7.8	118	82	10.2	4.4	8.0	1.9	77	0.5	5.1	0.08	0.15	0.01	61	44
Std. Dev.	19.4	5.6	0.3	34	25	2.3	1.6	2.6	0.6	18	0.2	1.5	0.11	0.07	0.01	16	12
							10265	150 Hot (Creek at !	- -							
Minimum	38.0	18.5	7.3	153	193	7.9	2.9	20.0	2.5	207	8.9	8.3	0.02	0.50	0.42	60	32
Maximum	283.0	37.0	8.7	591	406	13.0	6.3	100.0	9.0	234	57.0	32.0	3.90	2.50	2.60	192	58
Average	91.2	25.6	7.B	424	305	11.9	5.4	66.6	6.3	221	34.9	21.4	0.56	1.50	1.57	144	52
Std. Dev.	63.0	6.3	0.4	123	58	1.5	0.9	23.4	1.7	19	13.5	6.3	1.11	0.83	0.59	31	7
						3738221	18514401	003802	BE34R\$0	1M - AB	Bprings						
Minimum	2.5	15.5	7.1	212	184	9.4	7.1	21.0	4.5	104	7.1	9.1	0.21	0.20	0.36	85	53
Maximum	13.0	18.0	7.7	302	230	15.0	11.0	31.0	6.7	143	18.0	19.0	0.79	0.40	0.70	116	83
Average	5.7	16.9	7.3	267	197	13.1	9.5	26.8	5.8	130	11.8	13.3	0.37	0.30	0.54	107	72
Std. Dev.	2.9	0.7	0.2	22	17	1.6	1.1	2.9	0.6	11	2.9	2.5	0.13	0.06	0.11	8	8
						37381811	8513301	003802	ME36N84	13M - CD	Springs						
Minimum	5.7	14.0	7.1	185	154	11.0	8.0	21.0	4.4	120	3.8	9.4	0.24	0.10	0.20	98	60
Maximum	12.9	17.0	6.1	263	204	14.0	10.0	27.0	5.5	137	8.2	15.0	0.47	0.40	0.32	113	74
Average	8.3	15.6	7.5	237	179	12.2	9.2	23.9	5.1	131	58	11.1	0.34	0.31	0.27	107	68
Std. Dev.	1.5	0.6	0.3	16	10	0.7	0.5	1.3	0.3	4	1.1	1.2	0.06	0.06	0.03	3	4
						37382911		*****	F38K80		Sorinos						
						31362911	9540847	VV3\$02	COOKED.	· H23	ofn.q.0ge						
Minimum	2.6	10.0	6.9	166	106	16.0	5.2	13.0	3.0	93	. 5.2	5.0	0.25	0.10	0.09	73	61
Maximum	4.1	13.0	7.7	241	168	21.0	6.9	18.0	4.1	115	11.0	13.0	0.70	0.40	0.13	94	81
Average	3.2	11.3	7.3	205	145	17.4	5.9	15.4	3.6	102	7.5	11.6	0.41	0.20	0.11	82	66
Std. Dev.	0.4	0.5	0.2	20	15	1.4	0.5	1.4	0.3	7	1.5	1.3	0.13	0.06	0.01		6

Note flow values correspond to observed flows when water quality samples were taken

The TDS concentration at the AB spring averages about 197 mg/L and ranges from a low of 164 mg/L to a high of about 203 mg/L. The TDS concentration at the CD spring averages about 237 mg/L and ranges from a low of 185 mg/L to a high of about 263 mg/L. The TDS concentration at the H23 spring averages about 205 mg/L and ranges from a low 166 mg/L to a high of about 241 mg/L. Plots of TDS versus discharge are included in the appendix for each spring. There is a weak relationship between spring discharge and TDS for the AB spring. Linear regression for TDS as a function of discharge for each spring yielded the following parameters:

Spring	Slope	Intercept	Coefficient of Determination (R2)
AB	-3.80	218	0.3700
CD	-1.44	191	0.0454
H23	7.24	121	0.0328

About 37 percent of the variation in TDS in the AB spring can be attributed to variation in AB spring discharge. The TDS variations in the CD and H23 springs are not significantly influenced by variations in discharge at these springs.

The hardness at the AB spring averages about 72 mg/L (expressed as mg/L of CaCO3) and ranges from a low of 53 mg/L to a high of about 82 mg/L. The hardness at the CD spring averages about 68 mg/L and ranges from a low of 60 mg/L to a high of about 74 mg/L. The hardness at the H23 spring averages about 68 mg/L and ranges from a low 61 mg/L to a high of about 81 mg/L. Plots of hardness versus discharge are included in the appendix for each spring. There is a weak relationship between spring discharge and hardness for the AB and CD springs. Linear regression for hardness as a function of discharge for each spring yielded the following parameters:

Spring	Slope	Intercept	Coefficient of Determination (R2)
AB	-1.76	81	0.3367
CD	-1.60	81	0.4545
H23	6.18	48	0.1837

About 34 percent of the variation in hardness in the AB spring can be attributed to variation in AB spring discharge; 45 percent of the variation in hardness in the CD spring can be attributed to

variation in CD spring discharge; and 18 percent of the variation in hardness in the H23 spring can be attributed to variation in H23 spring discharge.

Total inorganic nitrogen concentration (expressed as mg/L of nitrogen) at the AB spring averages about 0.30 mg/L and ranges from a low of 0.28 mg/L to a high of about 0.31 mg/L. Total inorganic nitrogen concentration at the CD spring averages about 0.33 mg/L and ranges from a low of 0.28 mg/L to a high of about 0.39 mg/L. Total inorganic nitrogen concentration at the H23 spring averages about 0.43 mg/L and ranges from a low 0.26 mg/L to a high of about 0.68 mg/L. Ammonia levels range from <0.01 to 0.04 mg/L. Plots of total inorganic nitrogen versus discharge are included in the appendix for each spring. There is a weak relationship between spring discharge and total inorganic nitrogen for the AB spring. Linear regression total inorganic nitrogen a function of discharge for each spring yielded the following parameters:

Spring	Slope	Intercept	Coefficient of Determination (R2)
AB	0.0210	0.25	0.2162
CD	0.0048	0.30	0.0151
H23	-0.0099	0.44	0.0009

About 20 percent of the variation in total inorganic nitrogen in the AB spring can be attributed to variation in AB spring discharge. The total inorganic nitrogen variations in the CD and H23 springs are not significantly influenced by variations in discharge at these springs. Essentially all the total inorganic nitrogen is nitrate. The maximum contaminant level nitrate in drinking water is 10 mg/L as nitrogen. During the period of record, nitrate, as a component of total inorganic nitrogen, has always been measured far below the nitrate maximum contaminant level.

The phosphorus concentration (orthophosphate phosphorus) at the AB spring averages about 0.44 mg/L and ranges from a low of 0.34 mg/L to a high of about .049 mg/L. The phosphorus concentration at the CD spring averages about 0.52 mg/L and ranges from a low of .034 mg/L to a high of about 0.58 mg/L. The phosphorus concentration at the H23 spring averages about 0.3 mg/L and ranges from a low 0.25 mg/L to a high of about 0.34 mg/L. Plots of discharge versus phosphorus concentration are included in the appendix for each spring. There is no apparent relationship between flow and phosphorus. Linear regression for each spring yield coefficient of determinations of ranging from 0.0001 to 0.001.

The arsenic concentration at the AB spring averages about 0.047 mg/L and ranges from a low of 0.020 mg/L to a high of about 0.077 mg/L. The arsenic concentration at the CD spring averages about 0.052 mg/L and ranges from a low of 0.030 mg/L to a high of about 0.085 mg/L The arsenic concentration at the H23 spring averages about 0.022 mg/L and ranges from a low 0.015 mg/L to a high of about 0.048 mg/L. The maximum contaminant level for arsenic in drinking water is 0.050 mg/L. There are times when the discharge from the AB and CD headsprings are not potable. Plots of discharge versus arsenic concentration are included in the appendix for each spring. There is no apparent relationship between flow and arsenic. Linear regression for each spring yield coefficient of determinations ranging from 0.0005 to 0.03.

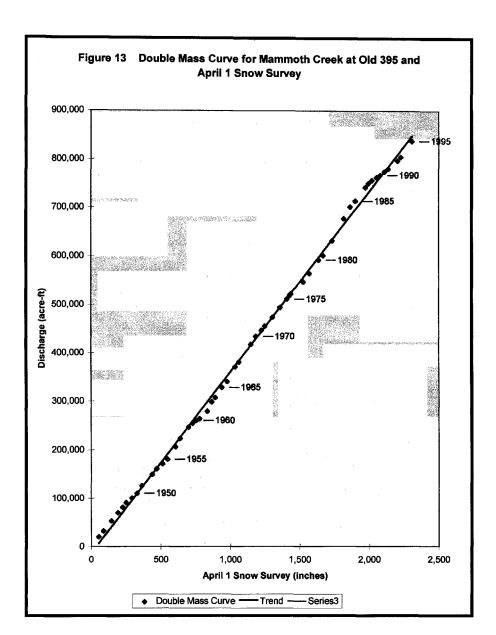
RELATIONSHIP BETWEEN HISTORICAL GROUNDWATER EXTRACTION AND DISCHARGE AT THE AB AND CD HEADSPRINGS

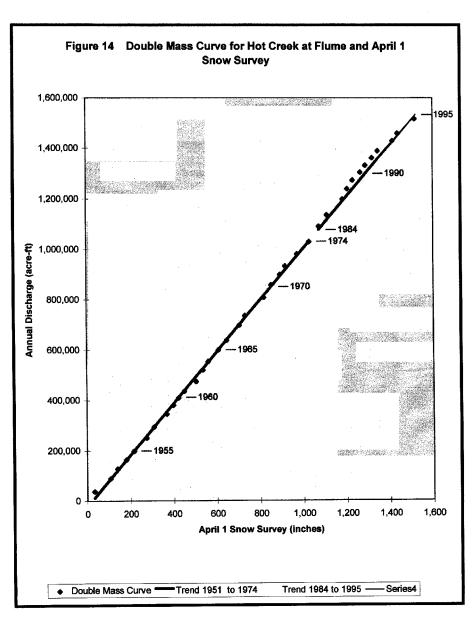
Prior investigations (USFS, 1990) presumed that groundwater extraction in the western part of the Mammoth Basin would cause a comparable reduction in spring flow at the headwater springs. Presumption of this impact is based on the assumption that groundwater storage is small, and that all groundwater eventually leaves the basin as surface flow in Hot Creek. If these assumptions were true then we should be able to observe groundwater level and stream discharge changes caused by groundwater extraction.

The groundwater extraction area in question is located about seven miles west and hydraulically up-gradient of the headsprings. Groundwater elevations in the vicinity of the significant groundwater extraction ranges from about 7,600 to 7,800 ft-msl. The groundwater elevation in the vicinity of the AB and CD headwater springs is about 7,075 ft-msl. A necessary condition for the groundwater extraction in the west Mammoth Basin area to influence the springs would be a change in the hydraulic gradient from the groundwater extraction area in the west extending continuously to the headsprings. Figure 6 shows a groundwater profile extending from the MCWD groundwater extraction area in the western part of the mammoth groundwater basin through the AB and CD headspring area. Plate 2 shows the groundwater level histories at wells extending from the MCWD groundwater extraction area in the west through the headspring area.

The drop in groundwater level in the groundwater extraction area due to pumping in the west can be clearly seen in and Plate 2 (pink hydrographs) to range between 40 to 60 feet during the period 1987 to 1992. Storage depletion during part of the drought can be seen in MCWD well hydrographs in the far western end of the groundwater basin. Some down-gradient monitoring wells with ambient groundwater elevations above 7,400 ft-msl show slight groundwater level declines during the drought and may have been influenced by the accumulated up-gradient groundwater extraction during the drought. Groundwater elevations and the gradient below groundwater elevation 7,300 ft-msl show no significant changes due to drought or up-gradient groundwater extraction. Review of groundwater level data in Figure 6 and Plate 2 show that aquifer stresses originating in the western part of the Mammoth Basin from groundwater extraction did not extend to the area of the headsprings where groundwater levels are about elevation 7,075 ft-msl.

The streamflow records for Mammoth Creek at Old 395 and Hot Creek at Flume were studied to see if groundwater extraction in the western part of the Mammoth Basin could have impacted the aggregate of spring flows. Double mass curves were developed for these stream discharge gaging stations. Double mass curves are plots of accumulative mass or flow at one station versus a similar accumulative term for another nearby station. Double mass curves are used to determine if significant changes have occurred at precipitation and stream discharge gages due to such activities as relocation of gages or construction of stream diversions. Changes in discharge due to drought or wet periods are filtered out in double mass curve analysis. Each point on the curve corresponds to a point in time. If data on the plot occurs after a change in the flow regime then the trend represented by the later data will diverge from the trend described by the data representing the period prior to a change. Figures 13 and 14 contain double mass curve plots for the Mammoth Creek at Old 395 gage versus April 1 snow survey, and the Hot Creek at the Flume gage versus the same index. Review of the Mammoth Creek plot shows a fairly straight line with no divergence. Groundwater extraction has not impacted the surface discharge measured at this location - groundwater levels are too deep to influence stream flows. The Hot Creek plot shows divergence corresponding to after 1986 -- the point in time that the drought occurred. If groundwater pumping were the source of the divergence, then the divergence would have been down to the right indicating that the stream discharge would be accumulating at a lessor rate than before significant groundwater extraction occurred. The Hot Creek mass curve diverges slightly





Basic Statistics — Double Mass for Hot Creek (2) 10/15/96

- 40 -

f

the opposite way, that is, Hot Creek coincidentally has more discharge than would historically have been expected, after significant groundwater extraction began. We checked with the USGS to see if there were any changes in flow measuring at the Hot Creek station that could have caused this apparent anomaly – they stated that to the best of their knowledge there were no such changes (telephone discussions with G. Rockwell of USGS, 7/30/96). The lack of downward divergence at the Hot Creek gage indicates that there has been no observed depletion of spring flows due to past groundwater pumping.

There is a significant amount of recent groundwater level data in the area between the MCWD groundwater extraction area in the western part of the Mammoth Basin and the AB and CD headwater springs. Review of the groundwater level data in Figure 6 and Plate 2 show that the changes in hydraulic gradient caused by groundwater extraction area in the western part of the Mammoth Basin did not extend to anywhere near the area of the headsprings. Review of the double mass curve for Hot Creek indicate that there has been no observed depletion of the aggregate spring discharge measured at the Hot Creek at the Flume gage. From these two observations we conclude that historical groundwater extraction in western part of the Mammoth Basin has not noticeably impacted the discharge at the AB and CD headspring.

The Mammoth Basin is hydrologically more complex than described by the simple conceptual model developed by the DWR in 1973. The DWR conceptual model of the Mammoth Basin was based on very simplistic assumptions, the most significant being that the yield of the Basin is directly equatable to average annual basin precipitation minus average consumptive use. Runoff, recharge and evapotranspiration processes are non linear with respect to precipitation — translated, average precipitation is not equatable to yield. The yield of the Mammoth groundwater basin can only be determined by studying hydrologic process over a historically-representative range of precipitation. Conceptual errors aside, the DWR analysis suffers from a lack of precipitation data, groundwater level and historical extraction data. The groundwater basin had never been significantly stressed prior to the late 1980's. The DWR estimated that the total outflow of the basin, surface and groundwater, to be about 40,600 acre-ft/yr. Based on review of historical groundwater levels, spring discharge and surface water discharge, the combined surface and groundwater yield of Mammoth basin should be much larger than the yield estimate developed by the DWR.

The DWR estimated that useful groundwater storage to be about 57,000 acre-ft based on groundwater stored only in unconsolidated deposits. In the 1980's MCWD developed extraction wells in fractured basalts which demonstrated that the useful storage includes fractured rocks that underlie and are adjacent to the unconsolidated deposits. The useful groundwater storage upgradient and tributary to the AB and CD headsprings is estimated to be about 242,700 acre-ft.

The lack of noticeable spring flow and stream flow depletions in the late 1980's and early 1990's is likely due to the yield being significantly larger than the MCWD groundwater extractions and AB and CD headspring discharges; and due to the large amount of storage relative to MCWD groundwater extractions and AB and CD headspring discharges. Yield in excess of MCWD groundwater extraction and spring discharge leaves the basin as subsurface outflow.

SECTION 3 FUTURE WATER DEMANDS AND SUPPLIES

CURRENT DEMANDS AND WATER SUPPLY SOURCES

Estimates of existing and future water demands in the Mammoth basin are listed in Table 8. These estimates are based in part on published estimates from MCWD (1996 Urban Water Management Plan, MCWD, May 1996) and other estimates for water users either not served by MCWD or not included in the 1996 Urban Water Management Plan. Table 9 shows the monthly demand pattern for water supplied by MCWD and the existing Snow Creek golf course.

Water supplies in the Mammoth lakes area comes from a combination of surface water diverted from Lake Mary and groundwater. Table 10 lists historical water extraction by MCWD (1983 to 1995) and groundwater extraction by the Snowcreek golf course. Domestic use at the Casa Diablo geothermal plant is estimated at 0.35 acre-ft/yr.

The capacity of MCWD supplies for existing conditions is:

Sources of Supply Existing System	Non Drought	Drought
Lake Mary	2,450	800
Well 1	500	315
GWTP1*	2,000	1,685
GWTP2**	1,500	1,450
Snowcreek G.W.	165	165
Total	6,615	4,415

^{*} MCWD wells 6, 10, 15 and 18 ** MCWD wells 16, 17 and 20

Table 8 Projected Water Demands for Mammoth Lakes Area Including Mammoth Community Water District and Adjacent Privately Served Lands (acre-ft/yr)

			(acie-suy)					
_		Existing \	Vater Demand		- Increment	al Demand to	Buildout -	Ultimat
Water Use Category	Units of Use	Number of Units of Use	Water Use per Unit (scre-ft/yr/unit)	Water Demand (ecre-ft/yr)	Units of Use	Number of Units of Use	Water Demand (acre-ft/yr)	Demand a Buildou (acre-fl/y
MCWD Municipal Service							·····	
Single Family Residential	edu	1,677	0.22	361	edu	707	152	51-
Condominium	edu	4,623	0.19	894	edu	1,544	298	1,19
Multi-Family/Apartment	edu	539	0.17	92	edu	470	80	17:
Mobile Home	edu	144	0.24	35	edu	11	3	3
Motel/Hotel	room	998	0.12	116	room	4,964	579	69
Commercial	RA	1,056,069	0.000161	170	R*R	379,642	61	23
Industrial	R°ft	106,635	0.000054	6	nn.	124,582	7	1:
Recreation/Parks	66	1	56.68	57	68	1	34	9.
Public Sector	88	1	20.48	20	68	1	12	3:
Irrigation (billed separately)	88	1	60.60	61	68	1	36	9
Other Residential	68	1	20.85	21	08	0	0	2
Fire Use, Maintenance	88	1	75.49	75	68	0	45	12
Audit Corrections	15%	of existing		286	10%	of existing	131	41
Conservation Devices		_					(111)	(111
Growth in Occupancy	25%	of existing +	audit corr.	549	25%	of existing 4	332	88
Subtotal MCWD Municipal Service				2,743			1,660	4.40
Other Demands								
Snowcreek Golf Course (1)				165			165	33
Lodester Golf Course (2)				0			300	30
Snowcreek Ski Area (3)				0			145	14
Geothermal Domestic(4)				0.35			0.12	0.4
Subtotal Other Demands				165			610	77
Total Ultimate Annual Demand Under Normal Climatic Conditions	.							5.17
Total Ultimate Annual Demand Under Drought Conditions (5)								3.00

Notes (1) Edsting 165 scra-flyr supplied by private wells, new 165 scra-flyr can be supplied with reclaimed water.

(2) Total demand will be met with reclaimed water when reclaimed water is available; MCWD will supply potable water until reclaimed water is available.

(3) 125 scra-flyr for snowmaking (50 af in Nov, 50 af in Dec and 25 af in Feb; 20 scra-flyr for domestic uses; and 125 scra-flyr for first 2 to 3 years for re-vegetation. Re-vegetation demand not included use along as before the snort term and small.

(4) Currently have are three gendermand plant in the area using a loale of about 0.5 scra-flyr. One more plant is proposed. Assume new plant uses about 0.12 acra-flyr (source Jim Anderson, plant manager for Mammoth Pacific, 8,8/96).

(5) Assumed water demands reduced by 25% during droughts.

Table 9 Monthly Water Demand by Water User Group

	Annual	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
	Allitual	Jali	FeU	THE STATE OF THE S	Aþi	may	Juli	Jui	Aug	Oep	Oct	1404	D
Basic Muni Demand	2,744	206	193	208	184	227	278	344	330	245	181	150	19
*	100.0%	7.5%	7.0%	7.6%	6.7%	8.3%	10.1%	12.5%	12.0%	8.9%	6.6%	5.5%	7.29
Ex. Snowcreek G.C.	165	0	0	0	0	23	28	34	34	28	18	0	1
Tot Dem, Norm Clim	2,909	206	193	208	184	250	306	378	364	273	199	150	19
Reclaimed Water Prod Norm Clim Cond	1,656	158	146	163	150	148	130	146	145	117	103	106	14
Ratio of Reci Wat Prod To Mun Supply		77%	75%	78%	81%	65%	47%	42%	44%	48%	57%	71%	739
Ultimate Demand Ti	me Histories												
	Annual	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
Basic Muni Demand	4,404	331	310	334	295	365	446	551	530	393	290	241	31
%	100.0%	7.5%	7.0%	7.6%	6.7%	8.3%	10.1%	12.5%	12.0%	8.9%	6.6%	5.5%	7.29
Lodestar GC	300	0	0	0	0	42	51	62	62	51	33	0	
Ex. Snowcreek G.C.	165	0	0	0	0	23	28	34	34	28	18	0	
Snowcreek GC Expension	165	0	0	0	0	23	28	34	34	28	18	0	_
nworeak snow making	125		25 4	0 2	0	0	0	0	0	0	0 2	50 3	5
worsek domestic	20	4	4	2	1	U	U	u	·	U	2	3	
Tot Dem, Norm Clim	5,179	335	339	336	296	452	553	681	659	500	361	294	37
Reclaimed Water Prod Norm Clim Cond	2,673	257	237	263	241	237	209	234	232	188	167	173	23
Ratio of Reci Wat Prod		77%	75%	78%	81%	65%	47%	42%	44%	48%	57%	71%	739

Table 10
Water Production by MCWD and Snowcreek
(scre-ttyr)

Year	MCW	D Production —		Snowcreek	Total
	Surface Water	Groundwater	Total	Groundwater Production	Groundwater Production
1983	2,221	48	2,269		48
1984	2,450	157	2,607		157
1985	2,196	313	2,509		313
1986	2,164	264	2,428		264
1987	1,537	563	2,100		563
1988	1,605	595	2,200		595
1989	1,780	958	2,738		958
1990	1,485	1,143	2,628		1,143
1991	1,048	1,337	2,385	27	1,364
1992	804	2,285	3,089	100	2,385
1993	1,653	1,677	3,330	37	1,714
1994	1,364	1,257	2,621	155	1,412
1995	1,726	968	2,695	165	1,133
verage	1,319	1,505	2,824	97	1,602
991 to 1995					

Source: MCWD Summary.ds

FUTURE WATER DEMANDS AND WATER SUPPLY SOURCES

Demands for ultimate buildout are listed in Table 8. These demand projections are based on the same references cited above for existing demand. The increase in water demand due to the expansion of the Snowcreek golf course from a 9-hole course to an 18-hole course, is estimated to be the same as the existing 9-hole demand – 165 acre-ft/yr. That is, upon completion of the expansion, the Snowcreek golf course demand will have increased from 165 to 330 acre-ft/yr. Ultimate demand is projected to be about 5,200 acre-ft/yr, an increase of about 2,200 acre-ft/yr or 73 percent.

Sources of Supply Ultimate Water System	Non Drought	Drought
Lake Mary	2,300	800
Well 1	500	315
GWTP1*	2,000	1,685
GWTP2**	1,500	1,450
Dry Creek (on line 2010 or se	ooner) 1,500	1,400
Snowcreek G.W.	330	330
Total	8,100	5,980
* MCWD wells 6 10 15 and 18		

^{*} MCWD wells 6, 10, 15 and 18 ** MCWD wells 16, 17 and 20

FUTURE WATER SUPPLY SCENARIOS

Two basic scenarios were developed to investigate the potential impacts of groundwater extraction in the Mammoth area for ultimate (corresponding cumulative impacts) and project specific (direct) impact of Snowcreek golf course expansion. These scenarios are distinguished by the inclusion or exclusion of the Dry Creek Project. The Dry Creek project is essentially an importation project to bring supplemental waters from outside the Mammoth Basin to meet future water demands. MCWD has completed extensive testing in the Dry Creek area to determine the integrity of the supply. MCWD is also investigating other importation projects to bring in additional supplies from outside the Mammoth Basin should the Dry Creek project not be

implemented. Sub-scenario's were developed to include or exclude the direct use of reclaimed water as a water supply for the Snowcreek golf course expansion and for the Lodestar golf course. The scenario's studied herein include:

- Scenario 1a Supplies for ultimate or buildout conditions comes from within and outside of the Mammoth Basin and exclude reclaimed water.
- Scenario 1b Supplies for ultimate or buildout conditions comes from within and outside of the Mammoth Basin and include reclaimed water.
- Scenario 2a Supplies for ultimate or buildout conditions comes from within the Mammoth Basin and exclude reclaimed water.
- Scenario 2b Supplies for ultimate or buildout conditions comes from within the Mammoth Basin and include reclaimed water.

A water supply allocation plan was developed for each scenario for drought and non-drought conditions. The supply allocation plan is listed in Table 11. Table 11 also lists the annual Mammoth Basin groundwater extraction, ratio of supply to demand, additional (new) Mammoth Basin groundwater extraction, and the incremental Snowcreek demand for potable supplies. Total Mammoth Basin groundwater extraction is projected to range from a low of about 900 acre-ft/yr for Scenario 1b (includes Dry Creek and direct use of 465 acre-ft/yr of reclaimed water) to a high of 3,780 acre-ft/yr for Scenario 2a (excludes Dry Creek and direct use of reclaimed water).

Baseline groundwater extraction, as used herein, is the annual groundwater extraction representative of existing conditions. Groundwater extraction in excess of the baseline groundwater extraction is additional groundwater extraction due to the increased water demands (including expansion of the Snowcreek golf course) and or drought conditions. Baseline groundwater extraction is estimated to be 2,385 acre-ft/yr which is the largest annual groundwater extraction to occur in Mammoth Basin. Additional new groundwater extraction is projected to range from a low of about -1,500 acre-ft/yr for Scenario 1b (includes Dry Creek and direct use of 465 acre-ft/yr of reclaimed water) to a high of 1,400 acre-ft/yr for Scenario 2a (excludes Dry Creek and direct use of reclaimed water). The negative value of additional groundwater extraction means that local groundwater extraction declined from the baseline.

Table 11
Water Sources and Allocation for MCWD

Sources of Supply	Scenario 1a With Dry Creek No Reclamation		Scenario 1b With Dry Creek With Reclamation		Scenar No Dry No Recta	Creek	Scenario 2b No Dry Creek With Reclamation		
	Non- Drought	Drought	Non- Drought	Drought	Non- Drought	Drought	Non- Drought	Drough	
			Sources of	Supply		-			
Lake Mary	2,300	800	2,300	800	2,300	800	2,300	80	
Well 1	500	315	500	315	500	315	500	31	
GWTP1	2,000	1,685	2,000	1,685	2,000	1,685	2,000	1,68	
GWTP2	1,500	1,450	1,500	1,450	1,500	1,450	1,500	1,45	
Dry Creek Wells	1,500	1.400	1,500	1,400	0	0	0	•	
Reclamation	0	0	465	465	0	0	465	46	
Private Wells	330	330	165	165	330	330	165	16	
Total Supplies	8,130	5,980	8,430	6,280	6,630	4,580	6,930	4,88	
Total Mammoth GW	4,330	3,780	4,165	3,615	4,330	3,780	4,165	3,61	
		Ali	location of	Supplies					
Lake Mary	2,300	800	2,300	800	2,300	800	2,300	80	
Well 1	131	242	94	214	319	315	281	31	
GWTP1	524	1,294	374	1,147	1,274	1,685	1,124	1,68	
GWTP2	393	1,113	281	987	956	1,450	843	1,45	
Dry Creek Wells	1,500	1,400	1,500	1,400	0	0	0		
Reclamation	0	0	465	465	0	0	465	46	
Private Wells	330	330	165	165	330	330	165	16	
Total Allocated	5,179	5,179	5.179	5,179	5.179	4.580	5.179	4.88	
Total Mammoth GW	1,379	2,979	914	2,514	2,879	3,780	2,414	3,61	
Ratio of Supply to Demand	100%	100%	100%	100%	100%	88%	100%	94	
Baseline Groundwater Production	2,385	2,385	2,385	2,385	2,385	2,385	2,385	2,38	
Additional Groundwater Production	(1007)	593	(1472)	128	493	1395	28	123	
Incremental Snowcreek Potable Demand	165	165	0	0	165	165	0		
Increment of Additional Groundwater Prod Due to SnowCreek Golf Course Exp.	NA	28%	NA	0%	33%	12%	0%	01	

Water Demands for Build Rev -- Sources 9/20/96

The incremental Snowcreek potable demand is the additional demand required by the expansion of the Snowcreek golf course when reclaimed water is not available. This demand is either 165 acre-ft/yr or zero – 165 acre-ft/yr when reclaimed water is not available and zero when reclaimed water is available.

The ratio of supply to demand is ratio of available supply to demand. A value of less than 100 percent means that a shortage occurred. During the period of 1987 to 1992, demand was reduced from 65 to 75 percent of normal. In the present analysis, shortages occur only Scenarios 2a and 2b during drought conditions, due to the exclusion of Dry Creek Project. It is assumed that under shortage conditions, MCWD will impose waster use restrictions up to a maximum of 25 percent of normal water use.

Tables 12a through 12d show the water supply allocations on a monthly basis, monthly use of Mammoth Basin groundwater and the monthly flow of reclaimed water to Laurel Pond.

Table 12a Monthly Water Supply Allocations for Scenario 1a (acre-ft)

Scenario 1a	Ultimate Bulid	out, Dry C	reek Oper	rational, i	io Reclar	nation, an	id Non-De	ought Co	nditions				
Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
Lake Mary	2,300	192	192	192	179	192	192	192	192	192	192	178	19
Well 1	131	2	3	2	0	11	23	37	34	16	1	0	
GWTP1	524	9	11	10	0	45	90	148	137	64	4	0	3
GWTP2	393	7	8	7	0	34	68	111	103	48	3	0	2
Dry Creek Wells	1,500	125	125	125	117	125	125	125	125	125	125	116	11
Reclamation	0	0	0	0	0	0	0	0	0	0	0	0	
Private Wells	330	0	0	0	0	46	56	68	68	56	36	0	-
Total Supplied	5,179	335	339	336	296	452	553	681	659	500	361	294	37
Mammoth GW	1,379	18	22	20	0	136	237	365	343	183	44	0	6
Reci Water to Laurel Pond	2,673	257	237	263	241	237	209	234	232	188	167	173	23
Scenario 1a	Ultimate Build	out, Dry Co	reek Oper	rational, f	io Recian	nation, an	d Drough	rt Conditi	on				
Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
nke Mary	800	67	67	67	67	67	67	67	67	67	67	67	6
ell 1	242	14	14	14	10	20	29	39	37	24	13	10	1
GWTP1	1,294	74	76	75	55	109	153	210	199	127	69	54	9
GWTP2	1,113	64	65	64	47	94	132	181	171	110	59	46	7
Dry Creek Wells	1,400	117	117	117	117	117	117	117	117	117	117	117	11
Reclamation	0	0	0	0	0	0	0	0	0	0	0	0	
Private Wells	330	0	0	0	0	46	56	68	68	56	36	0	
Total Supplied	5,179	335	339	336	296	452	553	681	659	500	361	294	37
Mammoth GW	2,979	151	156	153	113	269	370	498	476	317	178	110	18
		257	237	263	241	237	209	234	232	188	167	173	23

Table 12b Monthly Water Supply Allocations for Scenario 1b (acre-ft)

Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
Lake Mary	2,300	192	192	192	179	192	192	192	192	192	177	178	19
Well 1	94	2	3	2	0	7	17	30	28	11	0	0	
GWTP1	374	9	11	10	0	28	69	121	110	42	0	0	2
GWTP2	281	7	8	7	0	21	52	91	83	32	0	0	2
Dry Creek Wells	1,500	125	125	125	117	117	117	117	117	117	115	116	12
Reclamation	465	0	0	0	0	65	79	96	96	79	51	0	
Private Wells	165	0	0	0	0	23	28	34	34	26	18	0	
Total Supplied	5,179	335	339	336	296	452	553	681	659	500	361	294	37
Mammoth GW	914	18	22	20	0	79	186	277	255	112	18	0	5
Reci Water to Laurel Pond	2,208	257	237	263	241	173	130	138	137	109	116	173	2
Scenario 1b	Ultimate Build	out, Dry C	reek Oper	ational, V	Vith Reci	amation,	Drought (Condition	18				
Scenario 1b	Ultimate Bullde Annual Allocation	out, Dry Ci Jan	reek Opei Feb	rational, V Mar	Vith Reci	ametion, May	Drought (Condition Jul	Aug	Sep	Oct	Nov	De
	Annual	•	-•	•		•	•		Aug 67	S e p 67	Oct 67	Nov 67	Di
Source ke Mary	Annual Allocation	Jan	Feb	Mar	Apr 67 10	May 67 17	Jun 67 24	Jul	Aug		67 10	67 10	
Source .ke Mary Well 1	Annual Allocation 800	Jan 67	Feb 67	Mar 67	Apr 67	May 67	Jun 67	Jul 67	Aug 67	67	67	67	
Source .ke Mary Well 1 GWTP1	Annual Allocation 800 214	Jan 67 14	Feb 67 14	Mar 67 14	Apr 67 10	May 67 17	Jun 67 24	Jul 67 34	Aug 67 32	67 19	67 10	67 10	
Source	Annual Allocation 800 214 1,147	Jan 67 14 74	67 14 76	Mar 67 14 75	Apr 67 10 55	May 67 17 88	Jun 67 24 129	Jul 67 34 180	Aug 67 32 169	67 19 102	67 10 53	67 10 54	
Source .ce Mary Well 1 GWTP1 GWTP2	Annual Allocation 800 214 1,147 987	Jan 67 14 74 64	67 14 76 65	Mar 67 14 75 64	Apr 67 10 55 47	67 17 88 76	Jun 67 24 129 111	Jul 67 34 180 155	Aug 67 32 169 146	67 19 102 88	67 10 53 46	67 10 54 46	
xe Mary Well 1 SWTP1 SWTP2 Dry Creek Wells Reclamation	Annual Allocation 800 214 1,147 987 1,400	97 14 74 64 117	67 14 76 65 117	67 14 75 64 117	67 10 55 47 117	67 17 88 76 117	Jun 67 24 129 111 117	50 67 34 180 155 117	Aug 67 32 169 146 117	67 19 102 88 117	67 10 53 46 117	67 10 54 46 117	
ke Mary Nell 1 GWTP1 GWTP2 Dry Creek Wells	Annual Allocation 800 214 1,147 987 1,400 465	Jan 67 14 74 64 117	67 14 76 65 117	67 14 75 64 117	Apr 67 10 55 47 117	67 17 88 76 117 65	Jun 67 24 129 111 117 79	54 180 155 117 96	67 32 169 146 117 96	67 19 102 88 117	67 10 53 46 117 51	67 10 54 46 117	1
ke Mary Nell 1 SWTP1 SWTP2 Dry Creek Wells Reclamation Private Wells	Annual Allocation 800 214 1,147 987 1,400 485 165	57 14 74 64 117 0	67 14 76 65 117 0	67 14 75 64 117 0	67 10 55 47 117 0	67 17 88 76 117 65 23	Jun 67 24 129 111 117 79 28	54 180 155 117 96 34	67 32 169 146 117 96 34	67 19 102 88 117 79 28	67 10 53 46 117 51	67 10 54 46 117 0	1

Table 12c Monthly Water Supply Allocations for Scenario 2a (acre-ft)

Scenario 2a	Ultimate Build	out, No Dr	/ Creek P	Toject, No	Reclam	ition, and	Non-Dro	ught Con	ditions				
Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
ake Mary	2,300	192	192	192	192	192	192	192	192	192	192	192	192
Vell 1	319	20	21	20	15	24	36	51	48	29	14	14	20
SWTP1	1,274	81	84	82	59	98	144	204	191	114	57	58	10
SWTP2	956	61	63	61	44	73	108	153	144	86	43	43	7
Ory Creek Wells	0	0	0	0	0	0	0	0	0	0	0	0	
Reclamation	0	0	0	0	0	0	0	0	0	0	0	0	
Private Wells	330	0	0	0	0	46	56	68	68	56	36	0	
otal Supplied	5,179	354	359	356	310	434	536	667	643	476	342	307	39
Mammoth GW	2,879	162	167	164	118	242	345	476	451	284	150	116	20
Reci Water to Laurel Pond	2,673	257	237	263	241	237	209	234	232	188	167	173	23
icenario 2a	Uitimate Build	out, No Dry	Creek P	roject, No	Recima	ion and C	rought C	onditions	3				
Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
xe Mary	800	67	67	67	67	67	67	67	67	67	67	67	6
Vell 1	315	22	22	22	20	26	32	39	38	28	21	19	2
WTP1	1,685	118	120	119	104	140	171	211	203	152	112	104	13
SWTP2	1,450	102	103	102	90	120	147	182	175	131	96	89	11
Dry Creek Wells	0	0	0	0	0	0	0	0	0	0	0	0	
Reclamation	0	0	0	0	0	0	0	0	0	0	0	0	
Private Wells	330	0	0	0	0	46	56	68	68	56	36	0	
otal Supplied	4,580	308	311	309	281	399	473	567	551	434	332	279	33
fammoth GW	3,780	242	245	243	214	332	406	500	484	368	265	212	26
RecI Water to	2,364	227	209	233	213	210	185	207	206	166	147	153	20

Table 12d Monthly Water Supply Allocations for Scenario 2b (scre-ft)

		out, No Dr	Creek P	roject, W	ith Recia	mation, a	nd Non-D	rought Co	onditions				
Source	Annual Allocation	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
Lake Mary	2,300	192	192	192	192	192	192	192	192	192	192	192	19
Well 1	281	18	18	18	13	22	32	45	42	25	13	13	2
GWTP1	1,124	72	74	72	52	86	127	180	169	101	50	51	9
GWTP2	843	54	55	54	39	65	96	135	127	76	38	38	6
Dry Creek Wells	0	0	0	ō	Ō	0	O	0	0	O	0	0	
Reclamation	465	Ŏ	ō	ō	ō	65	79	96	96	79	51	ō	
Private Wells	165	ō	Ō	Ō	Ō	23	28	34	34	28	18	ō	i
Total Supplied	5.179	335	339	336	296	452	553	681	659	500	361	294	37
Mammoth GW	2,414	143	147	145	105	196	283	394	372	229	118	102	18
Reci Water to Laurel Pond	2,208	257	237	263	241	173	130	138	137	109	116	173	23
Scenario 2b	Ultimate Build	out, No Dr	/ Creek P	roject, W	ith Recia	mation, a	nd Drougi	ht Condit	ions				
Source	Annual	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	De
	Allocation												-
' ake Mary	Aflocation 800	67	67	67	67	67	67	67	67	67	67	67	6
' વke Mary કો 1		67 24	67 24	67 24	67 21	67 25	67 30	67 37	67 38	67 26	67 20	67 21	6
all 1	800	•											6 2
الدُ WTP1ئ	800 315	24	24	24	21	25	30	37	36	26	20	21	6 2 14
' ake Mary all 1 GWTP1 GWTP2 Dry Creek Wells	800 315 1,685	24 128	24 129	24 128	21 113	25 132	30 162	37 200	36 191	26 141	20 106	21 112	6 2 14 12
ਭੀ 1 GWTP1 GWTP2 Dry Creek Wells	800 315 1,685 1,450	24 128 110	24 129 111	24 128 111	21 113 97	25 132 114	30 162 139	37 200 172	36 191 165	26 141 122	20 106 91	21 112 97	6 2 14 12
all 1 GWTP1 GWTP2 Dry Creek Wells Reclamation	800 315 1,685 1,450 0	24 128 110 0	24 129 111 0	24 128 111 0	21 113 97 0	25 132 114 0	30 162 139 0	37 200 172 0	36 191 165 0	26 141 122 0	20 106 91 0	21 112 97 0	6 2 14 12
الد GWTP1 GWTP2	800 315 1,685 1,450 0 485	24 128 110 0	24 129 111 0	24 128 111 0	21 113 97 0	25 132 114 0 65	30 162 139 0 79	37 200 172 0 96	36 191 165 0 96	26 141 122 0 79	20 106 91 0 51	21 112 97 0	
all 1 GWTP1 GWTP2 Dry Creek Wells Reclamation Private Wells	800 315 1,685 1,450 0 465 165	24 128 110 0 0	24 129 111 0 0	24 128 111 0 0	21 113 97 0 0	25 132 114 0 65 23	30 162 139 0 79 28	37 200 172 0 96 34	36 191 165 0 96 34	26 141 122 0 79 28	20 106 91 0 51 18	21 112 97 0 0	6 2 14 12

SECTION 4

IMPACT OF NEW GROUNDWATER EXTRACTION ON HOT CREEK HEADSPRINGS

ASSUMPTIONS AND METHODOLOGY

It was concluded in Section 2 that there has been no discernible impact on Hot Creek headsprings from historical groundwater extraction in the western part of the Mammoth Basin. The hydrologic and geologic complexities of the Basin preclude the development and use of precise groundwater flow model for impact analysis. A conservative approach was developed to estimate impacts of future new groundwater extraction on the headsprings. We assumed that all new groundwater extraction would impact the springs directly with the impact allocated to the springs based on their relative contribution to the Hot Creek base flow. Groundwater extraction impacts would normally be buffered or attenuated due to groundwater storage – we assumed attenuation from storage to be negligible. We further assumed that the seasonal variation in groundwater extraction would not propagate through the groundwater basin to the headsprings. This assumption is reasonable due to the great distance between the extraction area and the headsprings (about 7 miles) and the observation that the historical extraction has not noticeably influenced the headsprings.

The results of this analytical approach is shown in Table 13. New extraction, if positive, is assumed to deplete the springs with 18 percent allocated to the AB spring, 23 percent to the CD spring and 9 percent to H23 spring. The remaining depletion is assumed to occur in aggregate at other springs from the Hot Creek Fish Hatchery to the Hot Creek gage. This is a "worst' case analysis in that spring flows are assumed to respond immediately and in direct proportion to new groundwater extraction.

IMPACTS ON SPRING DISCHARGE

Table 13 contains the average spring discharge in the column titled "non drought" and the

Table 13
Projected Worst-Case Impacts From Cumulative and Incremental
New Water Production MCWD Service and Surrounding Areas
Spring Discharge (cfs)

	Spring	Flow	Fraction of				- Flow in S	Springe			
	Non- Drought	Drought	Spring Flow Depletion Assigned to Spring	Scenario With Dry (No Reclan	Creek	Scenar With Dry With Reci Non-	Creek	No Dry No Recis Non-	Creek	Scenar No Dry With Reci Non-	Creek
			to apring	Drought	Diougni	Drought	Drought	Drought	Drought	Drought	Drougn
Cumulative New Groundwater Production				(1,007)	593	(1,472)	128	493	1,395	28	1,230
New Snowcreek Production				165	165	0	0	165	165	0	(
AB Spring	6.5	2.1	18%								
Cumulative				ne	2.0	ne	2.1	6.4	1.8	8.5	1.8
Snowcreek				ne	2.1	na	2.1	6.4	2.1	8.5	2.1
CD Spring	8.3	5.5	23%								
Cumulative Snowcreek				na na	5.3 5.4	na na	5.5 5.5	8.2 8.3	5.1 5.4	8.3 8.3	5.1 5.8
1100 feeder	3.3	2.4	9%								
H23 Spring Cumulative	3.3	2.4	9%	na	2.3	па	2.4	3.2	2.2	3.3	2.2
Snowcreek				ne	2.4	ne	2.4	3.3	2.4	3.3	2.4
All Other Springs Below Hot Creek Fish Hatchery	19.7	8.8	50%								
Cumulative Snowcreek				na na	8.4 8.7	na na	8.7 8.8	19.4 19.6	7.8 8.7	19.7 19.7	8.6 8.6
Total All Springs (1) Cumulative Snowcraek	37.8	18.8		na na	18.0 18.6	na na	18.6 18.8	37.2 37.6	16.9 18.6	37.8 37.8	17. ⁻ 18.i

⁽¹⁾ Base flow for Hot Creek at Flume form Table 6.

estimated lowest average daily discharge observed at the spring in the column titled "drought." The spring flow depletions, assumed to occur due to new groundwater extraction, are deducted from these flows for the cumulative new groundwater extraction and the incremental extraction from expansion of Snowcreek golf course. The resulting spring discharge are listed in Table 13. The cumulative impacts vary with scenario and climatic assumptions, ranging from zero up to 0.4 cfs at individual springs. The incremental impacts of the Snowcreek golf course expansion are always less than 0.1 cfs at individual springs. These impacts are conservative, will probably be much less than estimated herein, and most likely not measurable.

IMPACTS ON SPRING DISCHARGE TEMPERATURE

A linear relationship for temperature for the AB spring discharge as a function of discharge was developed by regression and is described in Section 2. This relationship was used to estimated the spring discharge temperature when groundwater extractions are increased in the future. Table 14 lists the estimated spring discharge temperatures for average and drought discharge conditions, for the Snowcreek golf course expansion and for ultimate buildout conditions. For the AB, CD and H23 springs, cumulative and incremental temperature impacts for all scenarios range from zero to less than 0.1 degrees-C for all water development scenarios.

IMPACTS ON SPRING DISCHARGE WATER QUALITY

Tables 15, 16 and 17 lists the projected TDS, hardness and total inorganic nitrogen concentrations in spring discharges, for average and drought discharge conditions, for the Snowcreek golf course expansion and for ultimate buildout conditions. The estimated TDS, hardness and total inorganic nitrogen concentrations are based on the linear regressions described in Section 2. The TDS and hardness concentrations change by 1 mg/L or less for all water development scenarios. The total inorganic nitrogen changes than 0.1 mg/L or less for all water development scenarios. The coefficient of determination phosphorous and arsenic are so low that the projected change in discharge of the springs due to new groundwater extraction will have no impact on their respective concentrations.

Table 14

Projected Worst-Case impacts From Cumulative and Incremental New Water Production MCWD Service and Surrounding Areas Temperature (degrees Centegrade)

	Spring	Flow	Fraction of			T	enutanegme	in Springs			
	Non- Drought	Drought	Spring Flow Depletion Assigned to Spring	Scenar With Dry No Recta Non- Drought	Creek	Scenar With Dry With Red Non- Drought	Creek	Scene No Dry No Reck Non- Drought	Creek	Scena No Dry With Red Non- Drought	Creek
AB Spring Cumulative Snowcreek	16.7	17.5	18%	na na	17.5 17.5	na na	17.5 17.5	16.6 16.7	17.6 17.5	18.7 16.7	17.6 17.5
CD Spring Cumulative Snowcreek	15.6	15.2	23%	na na	15.2 15.2	na na	15.2 15.2	15.6 15.6	15.2 15.2	15.6 15.6	15.2 15.2
H23 Spring Cumulative Snowcreek	11.3	11.1	9%	ne ne	11.1 11.1	në në	11.1 11.1	11.3 11.3	11.0 11.1	11.3 11.3	11.0 11.1

Table 15
Projected Worst-Case impacts From Cumulative and incremental
New Water Production MCWD Service and Surrounding Areas
Total Dissolved Solids (mg/L)

	Spring		Fraction of				Dissolved S				
	Non- Drought	Drought	Spring Flow Depletion Assigned to Spring	Scenar With Dry No Recta Non- Drought	Creek	Scenar With Dry With Reci Non- Drought	Creek	Scena No Dry No Recis Non- Drought	Creek	Scena No Dry With Rec Non- Drought	Creek
AB Spring Cumulative Snowcreek	194	210	18%	ne ne	211 210	ne ne	210 210	194 194	211 210	194 194	211 210
CD Spring Cumulative Snowcreek	179	184	23%	na na	184 184	ne ne	184 184	180 180	184 184	179 179	184 184
H23 Spring Cumulative Snowcreek	145	139	9%	nė ne	138 139	na na	139 139	145 145	138 139	145 145	138 139

Table 16
Projected Worst-Case Impacts From Cumulative and Incremental
New Water Production MCWD Service and Surrounding Areas
Hardness (mg/L as CaCO3)

	Spring	Flow	Fraction of				Hardness is	Springs -			
	Non- Drought	Drought	Spring Flow Depletion Assigned to Spring	Scena With Dry No Reck Non- Drought	y Creek	Scenar With Dry With Red Non- Drought	Creek	Scenar No Dry No Recia Non- Drought	Creek	Scenar No Dry With Red Non- Drought	Creek
AB Spring Cumulative Snowcreek	70	78	18%	ne ne	78 78	në në	78 78	70 70	78 78	70 70	78 78
CD Spring Cumulative Snowcreek	68	73	23%	ne ne	73 73	na na	73 73	68 68	73 73	68 68	73 73
H23 Spring Cumulative Snowcreek	68	63	9%	na na	62 63	ne ne	63 63	68 68	62 63	68 68	62 63

Table 17
Projected Worst-Case Impacts From Cumulative and Incremental
New Water Production MCWD Service and Surrounding Areas
Total Inorganic Nitrogen (NH3+NO2+NO3 as mg/L of N)

	Spring		Fraction of				Hardness is	Springs -			
	Non- Drought	Drought	Spring Flow Depletion Assigned to Spring	Scenar With Dry No Recla Non- Drought	Creek	Scenar With Dry With Red Non- Drought	Creek	Scena No Dry No Reck Non- Drought	Creek	Scena No Dry With Red Non- Drought	Creek
AB Spring	0.39	0.29	18%								
Cumulative Snowcreek				ne ne	0.29 0.29	na na	0.29 0.29	0.38 0.39	0.29 0.29	0.3 9 0.39	0.29 0.29
CD Spring	0.34	0.32	23%								
Cumulative .				na	0.32	ne	0.32	0.33	0.32	0.33	0.32
Snowcreek				na	0.32	nė	0.32	0.33	0.32	0.34	0.32
H23 Spring	0.41	0.42	9%								
Cumulative				ne	0.42	ne	0.42	0.41	0.42	0.41	0.4
Snowcreek				ne	0.42	na	0.42	0.41	0.42	0.41	0.43

SECTION 5 REFERENCES

Barnett Consultants, spring flow data in hardcopy format.

Beak Consultants, Incorporated, Brown Trout and Rainbow Trout Instream Flow Requirements in Mammoth Creek, California, draft report, September 1991.

Department of Water Resources (DWR), Mammoth Basin Water Resources Environmental Study, December 1973.

Kenneth Schmidt and Associates, Results of the Summer 1993 aquifer test, Mammoth County Water District Well No. 15, November 1993.

Kenneth Schmidt and Associates, Letter report regarding Potential Impacts of MCWD Well No. 11 Pumpage, March 27, 1991.

Kenneth Schmidt and Associates, Annual Report on Results of Mammoth Community Water District Groundwater Monitoring Program for October 1994 to September 1995, December 1995

Leroy Crandall and Associates, Review of Available Information on Ground Water Conditions in Mammoth Valley, May 1991.

Los Angeles Department of Water and Power (LADWP), streamflow data in hardcopy and magnetic forms for Mammoth Creek at Old 395 and Hot Creek at Flume.

Mammoth Community Water District (MCWD), 1996 Urban Water Management Plan, May 1996.

Triad Engineering Corporation, Watershed Analysis for Proposed Sherwin Ski Area, December 1985

United States Department of Agriculture, Forest Service, Draft Environmental Impact Statement, Proposed Snowcreek golf Course Expansion Project, December 1995.

United States Geological Survey (USGS), Sources of Arsenic in Streams Tributary to lake Crowley, California, 1976.

United States Geological Survey (USGS), Hydrologic and Geochemical Monitoring in Long Valley Caldera, Mono County California, 1982 to 1984, Water-Resources Investigations Report 85-4183, 1985.

United States Geological Survey (USGS), Hydrologic and Geochemical Monitoring in Long Valley Caldera, Mono County California, 1985, Water-Resources Investigations Report 87-4090, 1987.

United States Geological Survey (USGS), Review of Mammoth Community Water District Reports and Data, circa February 1995.

Appendix

Water Quality Data At Selected Stream and Spring Locations (Data from USGS)

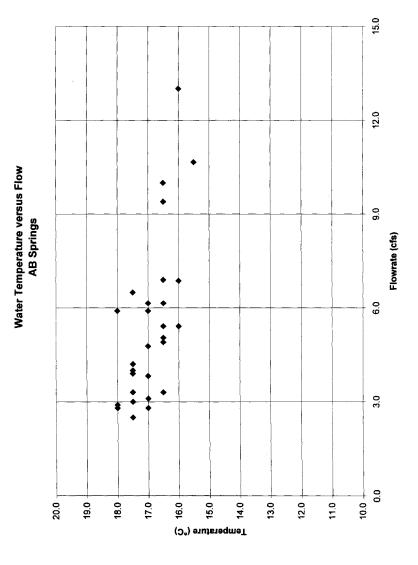
																		_					_
Date	Flow (cfs)	Water Temp (°C)	рН	EC (umho/em	TDS (mg/l)	Ca (mg/l)	Mg (mg/l)	ations — Na (mg/l)	K (mg/l)	HCC3 (mg/l)	CI (mg/l)	504 (mg/l)	NO3-N N-EON (N Rgm)	F (mg/l)	B (mg/l)	Tol Cations (meg/l)	Anions (meg/l)	Error (%)	Total Alkalinity (mg/l as	Total Hardness CACO3)	Inorganic Nitrogen (mg/l)	Ortho Phosph (mg/l)	As (ug/l)
	-						-		1026	5130 M	ammoth	Creek	nt Old 39	5									
8/14/83 10/3/83	78.9 37.5	12.0 8.0	7.8 7.8	55 89	55	5.1 7.4	1.7 2.7	3.4 5.2	1.1 1.3		0.4	≪5 3.5		≺0.1 0.10	<0.01 0.01				39	20 30			5
11/2/83 12/15/83	20.4	6.D 1.5	7.6 8.4	89 102	77 78	8.2 11.0	3.5 4.2	6.2 7.1	1.7		1,2	4.9 5.1		<0.1 0.30	0.05 0.01				47	37 45			2
1/17/84	15.5	0.5	7.8	150	100	12.0	5.6	8.8	2.3		0.4	5.8		0.10	0.02					53			5
4/5/84 5/10/84	13.0 35.0	5.0 13.0	8.2 8.0	165 121	77	13.0 10.0	8.9 4.1	12.0 6.7	2.1		0.6	7.0 5.1		0.10	0.02				92 54	61 42	0.2 <0.1		8
6/20/64 7/24/64	76.3 45.3	14.5	7.6 8.1	58 58	33	5.7 6.1	1.4	2.8 3.5	0.7		0.3	3.1 3.5		<0.1	0.02 <0.01				28	20 23	<0.1 <0.1		≺1 2
9/2/84	13.7	13.5	7.9	74	81	7.3	2.6	5.8	1.6		<0.1	4.0		0.30	0.01				40	29	<0.1		4
10/10/84	18.4 15.6	10.5 2.0	7.8 8.4	128 140	69 85	11.0 12.0	4.4 5.1	7.2 8.9	1.9		0.5	4.8 5.4		<0.1 0.15	0.01 <0.01				58	48 51	<0.1		2
10/19/85	4.7	3.0	8.3	124	89	9.7	5.2	8.6	2.2		0.5	6.5		⊲ 0.1	0.01				64	46	<0.1		4
4/11/86 7/13/68	22.8 13.7	8.0 13.0	8.1 8.1	153 82	111 50	13.0 7.8	5.8 2.4	9.9 4.8	2.2 1.1		0.4	9.2 3.1	0.09	0.10	0.01 <0.01				73 42	56 29	<0.1 0.11	0.05	8
1/11/89	3.6	5.5	7.8 7.1	140 165	95 109	11.0 13.0	5.6 8.3	9.3	2.3		0.4	5.8 6.8		0.10	<0.01 0.02				73 78	51 58	<0.1 <0.1	0.09	4
4/11/88	8.8	5.5	7.8	143	108	11.0	6.0	11.0	2.4		0.4	6.3		0.20	0.01				69	52	0.01	0.18	21
7/18/89 10/18/89	7.8 3.7	13.5 4.0	7.B 7.B	90 137	86 76	8.5 11.0	2.9 4.8	5.8 9.3	1.2		1.0	4.0 6.0		0.10	<0.01 0.81				49	33 47	0.02 <0.1	0.03	4 3
1/9/80	4.0		7.8	143	116	14.0	5.2	11.0	3.0		0.4	6.0		0.10	0.01				86	61	0.02	0.12	28
4/25/90 7/17/90	10.3	3.0 17.5	7.8	124 84	88 63	10.0 8.5	4.7 2.8	8.5	2.0	54	0.5 <0.1	5.1 3.8	0.48	0.10	<0.01 <0.01	0.94	0.97	3%	64 45	44 33	0.5	0.12	4
10/16/90	1.6	8.0	7.9	103	81	11.0	5.0	9.6	2.2	79	1.2	4.3		0.30	<0.01	1.44	1.43	0%	64	48	<0.1	0.12	3
1/17/91 4/18/91	1.4	1.0	7.7 7.9	165 161	89 109	14.0 13.0	6.4 6.7	12.0 13.0	2.8 2.8	98 99	0.2	5.9 7.4		<0.1 0.10	0.01 <0.01	1.82 1.84	1.74	5% 3%	81 82	61 60	0.04	0.12	4
7/22/91 0/22/91	15.5 3.2	17.0 9.5	8,1 7.7	71 118	46 66	7.8 9.7	2.1 4.4	4.9 7.5	1.0	41 77	<0.1 0.7	3.1 5.1		0.10	0.02 <0.01	0.80	0.74 1.40	7% 14%	35 63	28 42	0.02	0.03	•
1/13/92	3.5	0.5	7.9	137	85	12.0	5.1	9.4	2.1	86	0.5	5.3		0.20	<0.01	1.48	1.54	4%	70	51	0.09	0.12	2
V14/92 7/6/92	5.3 10.1	10.0 15.0	8.1 7.9	159 86	108 48	12.0 8.3	6.8 2.6	13.0 5.3	2.6 1.1	98 49	0.1 <0,1	8.6 3.5		<0.1 <0.1	0.02 <0.01	0.89	1.75 0.88	2% 1%	80 42	58 31	0.02 0.01	0.18 0.06	5 2
0/19/92	3.3	9.5	7.7	121	99	11.0	4.3	7.9	2.0	76	0.4	4.3		0.10	<0.01	1.30	1.35	4%	62	45	0.02	0.06	3
1/25/93 4/12/93	2.9 7.1	4.5	7.8 8.0	121 161	80	11.0 12.0	4.4 6.3	8.3 12.0	1.9	77 96	0.4	5.4 7.2		0.10	<0.01 0.01	1.32	1.39	5% 3%	79	46 56	0.07	0.25	3 5
7/12/93	71.7	17.0	7.7	42	30	5.5 9.1	0.9	2.1	0.8		0.2	1.7		<0.1	0.01					18	0.02	0.06	2
10/13/93	9.2 6.1	9.0	7.6 7.4	101 126	7D 8B	11.0	3.7 5.0	5.1 8.9	1.6 2.1	74	0.3	4.1 5.0		0.10 ≺0.1	<0.01 <0.01	1.40	1.33	5%	49 60	38 48	0.03	0.05	3
4/12/94 7/11/94	7.4 10.1	2.0 18.0	7.5 7.6	148 86	108 54	12.0 8.1	8.1 2.7	10.0	2.3	92 48	0.4	6.0 3.5		0,10 <0.1	<0.01	1.60	1.65	3% 2%	75 40	55 31	0.03 <0.05	0.12	3
10/19/94	5.3	2.0	7.4	133	88	11.0	4,8	9.0	2.0	78	0.3	4.1		0.10	0.01	1.38	1.38	1%	64	47	<0.05	0.09	3
1/17/95 4/17/95	8.7 11.1	0.5	7.3 7.8	130 148	88 104	11.0 12.0	4.5 5.5	8.4 10.0	2.2	73 87	0.5 0.7	4.0 5.8		<0.1 0.10	0.02 0.01	1.34 1.54	1.31	2% 2%	60 71	46 53	0.06 0.06	0.0 9 0.12	3
io of Data Minimum	41 1.4	36 0.5	41 7.1	42 42	41 30	42 5.1	42	42 2.1	42 0.6	18 41	38 0.1	41 1.7	0.09	29 0.10	23 0.01				34 28	42 18	23 0.01	28 0.03	41
Maximum	76.9	18.0	8.4	185	136	14.0	8.9	13.0	3.0	99	1.2	9.2	0.48	0.30	0.05				86	61	0.50	0.25	29
Average Std. Dav.	16.2 19.4	8.3 5.6	7.8 0.3	118 34	82 25	10.2 2.3	1.6	8.0 2.8	1.9 0.6	77 18	0.5 0.2	5.1 1.5	0.29 0.28	0.15 0.07	0.01 0.01				61 16	12	0.11	0.11	5
									1	026515	Hot C	reek at l	Flume										
11/16/82	213.0	19.5 17.0	7.7 7.5	340 216	235	10.0	4.8	53.0 28.0	5.3 3.4		28.0 13.0	20.0 12.0		1.20	1.30					45 41			140 70
7/6/83 8/8/83	283.0 173.0	22.5 18.5	7.3	153 248		7.9 9.5	2.9	20.0 33.0	2.5		8.9 17.0	8.3 12.0		0.50	0.42				60	32			52 88
10/3/83	97.0	21.5	7.7	363	235	12.0	5.6	55.0	5.8		27.0	19.0		1.00	1.30				120	53			120
11/2/83	80.0 88.0	20.5 18.5	7.5 7.5	410 416	276 262	12.0	5.6 6.1	50.0 58.0	6,3 6.0		31.0 29.0	19.0		1.40	1.40				133	53 58			150
4/5/B4	80.0	23.5	7.6	490	331	13.0	6.3	77.0	7.B		41.0	25.0		1.90	1.80				151	58	0.33		170
5/10/84 8/20/84	89.0 114.0	25.5 21.0	7.6 7.5	444 297	288 193	13.0	5.9 4.5	64.0 44.0	8.1 4.1		34.0 23.0	24.0 15.0		1.80	1.50				139	57 43	0.15 <0.1		160
7/24/84 9/2/84	0.89 0.88	27.5 24.5	8.2 7.9	382 445	233 303	13.0	5.D 5.7	51.0 72.0	5.0 7.2		25.0 37.0	18.0 22.0		1.20	1.20				122 144	52 54	0.2		120
0/10/84	84.0	24.5	7.5	471	313	13.0	8.2	78.0	7.4		37.0	23.0		1.80	1.60				156	58	0.22		160
11/11/B4 10/19/85	70.0 49.0	24.0 32.5	8.6 8.0	460 552	311 362	13.0	5.B 5.B	77.0 93.0	7.5 7.8		39.0 51.0	23.0 26.0		1.70 2.20	1.90				158 168	57 57	3.9		150 240
4/12/88 7/27/87	74.0	25.0 36.0	7.6	447 579	306 369	12.0	6.2 4.0	69.0 95.0	6.3		40.0	18.0		1.80	1.60					56			180
7/12/88	53.0	34.0	7.7	470	323	12.0	5.6	78.0	7.0		50.0 40.0	30.0 24.0	0.41	1.60	2.30 1.70				140	57 53	0.29	0.49	230
7/19/89 7/18/80	43.0 38.0	37.0	7.8	586 581	388 408	13.0	5.7 6.0	98.0 100.0	8.2 9.0	234	52.0 57.0	28.0		2.40	2.30	5.72	6 4R	11%	171	56 57	0.12	0.52	270
7/8/92	40.0	33.5	7.9	561	348	12.0	5.9	96.0	7.3	207	54.0	31.0	0.14	2.50	2.40	5.45	5.92	9%	188	54	0.18	0.58	280
lo of Data Minimum	20 38.0	21	21	21 153	18 183	21	21 2.9	21 20.0	21 2.5	2	21	21	2	21	21				14	21	11	4	20
Auximum	283.0	16.5 37.0	7.3 8.7	591	406	7.8 13.0	5.3	100.0	9.0	207 234	8.9 57.0	8.3 32.0	0.14	0.50 2.50	0.42 2.60				60 192	32 58	0.02 3.90	0.49	52 280
Average Std. Dev	91.2 63.0	25.6 6.3	7.B	424 123	305 58	11.9	5.4	68.6 23.4	6.3	221	34.9 13.5	21.4	0.28	1.50	1.57				144	52	0.58	0,58	162
Average Std. Dev.	91.2 63.0	6.3	0.4	123	305 58	11.9	0.9	23.4	1.7	19	13.5	8.3	0.18	0.63	0.59				31	7	1,11	0,58	

Water Quality Data At Selected Stream and Spring Locations (Data from USGS)

										-,-	ata Iron			_								
Date	Flow (cfs)	Water Temp (°C)	piH	EC (umho/om	TDS (mg/l)	Ca (mg/l)	Mg (mg/l)	ntions — Na (mg/l)	K (mg/l)	HCO3 (mg/l)	CI (mg/l)	SO4 (mg/l)	NO3-N (mg/l N)	F (mg/l)	B (mg/l)		Anions (maq/)	Error (%)	Total Total Alkalinity Hardnes (mg/l as CACO3)	Inorganic Nitrogen (mg/l)	Ortho Phosph (mg/l)	As (ug/l)
								3738	1811851	3301	0038028	E35NS0	3M - CD	Spring								
10/21/88 1/10/89 41/2/89 10/10/89 10/10/89 10/10/89 10/10/89 10/10/89 10/10/89 10/10/89 10/10/89 10/20/81 10/20/81 10/20/81 10/20/81 10/20/81 10/10/80 10/10	7.4 935 9.5 9.7 9.7 7.7 7.7 7.7 7.7 7.7 7.7 7.7 7.7	15.0 14.0 15.5 15.0 15.5 15.5 16.0 16.0 16.0 16.5 16.5 17.0 15.5 17.0 15.5 18.5 17.0 18.5 18.5 18.5 18.5 18.5 18.5 18.5	7.4 7.5 7.5 8.0 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.7 7.4 7.8 7.7 7.4 7.8 7.5 7.7 7.4 7.8 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	185 229 231 236 232 213 243 233 222 246 255 243 244 250 256 214 250 257 257 257 257 257 257 257 257 257 257	181 171 181 188 154 180 182 187 183 176 183 176 184 182 204 180 180 186 186 186 188 188 188 188	12.0 12.0 12.0 12.0 12.0 12.0 12.0 13.0 13.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12	84.0 9.0 9.0 8.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9	24.0 22.0 23.0 24.0 24.0 25.0 26.0 26.0 26.0 26.0 27.0 27.0 23.0 24.0 25.0 25.0 26.0 26.0 26.0 26.0 26.0 26.0 26.0 26	4.4 5.7 5.1 5.5 5.1 5.1 5.2 5.1 5.2 5.3 5.3 5.3 5.5 5.5 5.5 5.5 5.5 5.5 5.5	127 131 131 130 135 130 132 129 132 137 132 133 136 133 134 133 133	4.5 5.6 5.7 5.2 7.0 6.3 8.0 8.1 7.3 4.5 5.9 6.7 4.3 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.3 6.5 5.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	11.0 11.0 11.0 11.0 11.0 11.0 11.0 11.0	0.28 0.32 0.39 0.32	0.30 0.40 0.30 0.40 0.30 0.30 0.30 0.40 0.4	0.23 0.24 0.28 0.27 0.26 0.27 0.32 0.27 0.32 0.30 0.30 0.30 0.30 0.30 0.30 0.20 0.2	2.50 2.52 2.85 2.55 2.55 2.54 2.54 2.54 2.52 2.54 2.54	2.54 2.59 2.59 2.63 2.70 2.70 2.80 2.81 2.71 2.64 10.39 2.45 2.65 2.60 2.50 2.50 2.50 2.50	2% 78% 1% 2% 5% 1% 62% 6% 1% 2% 6% 1% 2% 6% 1% 2% 6% 1% 2% 6% 1% 2% 6% 1	108 80 108 67 108 67 108 67 108 67 108 67 108 67 108 67 104 66 108 87 104 107 107 108 72 105 72 105 72 105 72 107 107 108 11 109 72 107 107 108 11 109 72 109 72 109 74	0.32 0.34 0.29 0.26 0.27 0.3 0.31 0.31 0.32 0.31 0.34 0.34 0.35 0.34 0.35 0.31 0.31 0.32 0.31 0.34	0.49 0.55 0.52 0.52 0.52 0.58 0.55 0.55 0.55 0.55 0.55 0.55 0.55	57 82 49 54 55 66 68 52 55 55 56 56 57 57 58 58 58 58 58 58 58 58 58 58 58 58 58
7/11/95 No of Data Minimum Maximum Average Std. Dev.	11.D 29 5.7 12.9 8.3 1.5	15.5 28 14.0 17.0 15.8 0.8	7.2 28 7.1 8.1 7.5 0.3	223 28 185 263 237 16	168 29 154 204 179 10	11.0 20 11.0 14.0 12.2 0.7	8.5 8.0 10.0 9.2 0.5	29 21.0 27.0 27.0 23.9 1.3	4.7 28 4.4 5.5 5.1 0.3	120 120 120 137 131 4	3.8 3.8 8.2 5.8 1.1	10.0 29 9.4 15.0 11.1 1.2	4 0.28 0.39 0.33 0.05	0.30 28 0.10 0.40 0.31 0.08	0.20 0.20 0.32 0.27 0.03	2.28	2.32	1%	98 62 25 29 98 80 113 74 107 68 3 4	0.41 29 0.24 0.47 0.34 0.08	0.46 0.34 0.58 0.52 0.05	45 29 30 85 52 9
								3738	2211851	4401 0	035028	E34R\$0	1M - AB	Spring								
6/21/84 4/8/86 7/11/86 7/11/86 1/10/16/88 1/10/86 1/10	10.7 10.7 8.9 5.4 5.4 8.2 6.2 6.2 6.2 6.3 3.3 3.3 3.3 3.3 3.1 2.5 4.0 2.5 4.0 9.5 4.0 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5	18.0 15.5 18.0 16.5 16.0 16.5 16.0 16.5 17.0 16.5 16.0 17.0 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5	7.1 7.3 7.4 7.5 7.4 7.5 7.7 7.2 7.3 7.4 7.5 7.3 7.3 7.4 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	251 255 270 267 272 278 284 280 254 285 302 274 276 288 288 288 288 288 288 288 288 288 28	167 211 167 201 162 202 204 162 202 201 215 203 227 216 168 200 216 168 200 216 168 200 216 168 200 216 168 200 216 168 200 216 168 200 201 201 201 201 201 201 201 201 201	13.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14	9.7 10.0 11.0 11.0 10.0 10.0 10.0 10.0 10	24.0 25.0 26.0 28.0 28.0 27.0 28.0 28.0 28.0 28.0 28.0 28.0 28.0 28	5.1 5.3 6.1 5.0 5.0 6.0 6.0 6.1 6.3 6.4 6.3 6.0 6.1 6.1 6.0 6.1 6.0 6.1 6.0 6.1 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	135 139 131 140 125 128 128 123 143 143 143 143 144 140 142 104	8.0 11.0 10.0 10.0 111.0 111.0 111.0 115.0 12.0 12.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	10.0 12.0 14.0 14.0 14.0 14.0 13.0 13.0 14.0 14.0 14.0 16.0 15.0 16.0 16.0 16.0 17.0 18.0 16.0 16.0 16.0 17.0 18.0 18.0 18.0 18.0 18.0 18.0 18.0 18	0.28	0.40 0.30 0.30 0.30 0.30 0.30 0.30 0.30	0.37 0.40 0.44 0.47 0.55 0.59 0.59 0.64 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.63 0.64 0.55 0.64 0.55 0.64 0.55 0.64 0.55 0.64 0.55 0.64 0.65 0.64 0.65 0.64 0.65 0.66 0.66 0.67 0.67 0.67 0.68	3.08 2.24 3.12 3.12 3.12 2.79 2.92 2.89 2.80 2.53 2.28 2.28 2.28 2.28 2.28 2.28 2.28 2.2	2.88 3.15 3.11 2.75 2.85 2.85 2.85 2.85 2.86 2.72 2.36 2.73 2.73 2.74 2.73 2.74 2.73 2.75 2.75 2.75 2.75 2.75 2.75 2.75 2.75	7%% 0%% 1%% 1%% 2%% 3% 4%% 3% 4%% 3%	73 111 73 114 80 80 80 80 80 80 80 80 80 80 80 80 80	0.36 0.45 0.36 0.37 0.32 0.27 0.33 0.31 0.31 0.31 0.31 0.31 0.4 0.53 0.29 0.39 0.39 0.30 0.31 0.31 0.4 0.53 0.4 0.53 0.4 0.53	0.46 0.43 0.40 0.43 0.46 0.45 0.46 0.45 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	208 98 5 5 156 26 50 48 99 2 59 50 48 45 77 38 50 53 47 50 55 57 40 47 44 44 43 52 52 45 46 42 43 48 35
Minimum Maximum Average Std. Dev.	2.5 13.0 5.7 2.9	15.5 18.0 18.9 0.7	7.1 7.7 7.3 0.2	212 302 267 22	164 230 197 17	9.4 15.0 13.1 1.8	7.1 11.0 9.5 1.1	21.0 21.0 28.8 2.9	4.5 8.7 5.8 0.8	104 143 130	7.1 18.0 11.8 2.9	9.1 19.0 13.3 2.5	0.28 0.31 0.30 0.02	0.20 0.40 0.30 0.05	0.36 0.70 0.54 0.11				27 35 85 53 116 83 107 72 8 8	0.21 0.79 0.37 0.13	0.34 0.49 0.44 6,84	20 77 47 10

Water Quality Data It Selected Stream and Spring Locations (Data from USGS)

Date	Flow	Water					С	ntions				A	nions —			— Tota	I Ion Bala	nce	Total	Total	Inorganic	Ortho	
	(cfs)	(°C)	pH	EC (umho/em	TDS (mg/l)	Ca (mg/l)	Mg (mg/l)	Ma (mg/li)	K (mg/l)	(mg/l)	CI (mg/l)	504 (mg/l)	NO3-N (mg/l N)	F (mg/l)	B (mg/l)	Cations (meq/l)	Anions (meg/l)	Error (%)	Alkalinity (mg/l as	Hardness CACO3)	Nitrogen (mg/l)	Phosph (mg/l)	(0
								37382	911850	5801 D	38020	35K50	M - H2,3	3 Spring	j•								
711/88	3.5	11.0	7.6	193	141	16.0	5.6	13.0	3.0		6.2	12.0		0.30	0.12					63	0.32	0.26	
0/18/88	3.2	11.0	7.4	187	143	16.0	5.9	15.0	3.2		5.4	12.0		0.20	0.09					84	0.29	0.28	
/10/89	3.1	11.0	7.4	182	137	16.0	5.4	13.0	3.4		5.4	12.0		0.20	0.09					62	0.29	0.28	
/11/89	3.1	11.0	7.4	180	139	16.0	5,4	13.0	3.3		5.4	12.0		0.20	0.10				73	62	0.33	0.31	
/20/89	3.3	11.0	7.2	190	156	16.0	5.5	14.0	3.5		5.4	11.0		0.30	0.11				77	63	0.27	0.26	
V18/89	3.2	11.0	7.3	190	122	16.0	5.3	14.0	3.5		5.6	11.0	0.26	0.20	0.10					62	0.27	0.31	
1/9/90	2.9	11.0	7.5	179	134	16.0	5.3	14.0	3.8		5.2	6.0	*	0.20	0.10				73	62	0.36	0.28	
24/90	2.8	11.0	7.4	199	147	18.0	5.6	15.0	3.5		7.1	13.0	0.68	0.20	0.11				74	63	0.7	0.31	
/17/80	3.1	11.5	7.3	192	150	17.0	6.5	15.0	3.4	94	8.0	11.0		0.10	0.10	2.04	2.01	2%	77	85	0.52	0.31	
V16V90	3.5	11.5	7.4	166	129	16.0	5.4	14.0	3.4	96	7.3	12.0		0.40	0.10	1.84	2.08	6%	79	82	0.3		
/16/91	3.1	11.5	7.3	177	105	15.0	5.2	14.0	3.2		5.7	11.0		<0.1	0.10					61	0.3	0.31	
16/91	3.0	11.0	7.4	190	146	16.0	5.4	15.0	3.5	93	6.8	11.0		0.20	0.11	1.99	1.87	1%	76	62	0.63	0.25	
/23/81	3.6	13.0	7.3	198	140	17.0	5.7	16.0	3.5	96	7.9	13.0		0.20	0.12	2.10	2.09	1%	79	66	0.54	0.28	
Y23/91	2.7	11.5	7.2	201	142	17.0	5.8	16.0	3.7	94	8.0	12.0		0.20	0.11	2.12	2.04	4%	75	86	0.56	0.25	
/14/92	2.6	11.5	7.3	200	116	17.0	5.6	15.0	3.5	95	7.0	12.0		0.20	0.11	2.05	2.03	1%	79	66	0.33	0.31	
/15/92	2.8	11.0	7.7	210	156	18.0	8.2	18.0	3.5	101	9.4	12.0		0.10	0.12	2.20	2.19	0%	82	70	0.5	0.31	
77/92	3.0	11.0	7.3	213	130	18.0	5.0	16.0	3.6	105	8.1	12.0		0.10	0.12	2.17	2.22	2%	84	89	0.42	0.31	
/20/92	2.8	11.5	7.2	210	167	18.0	5.9	16.0	3.7	104	8.3	12.0		0.20	0.11	2.18	2.21	2%	85	89	0.53	0.31	
28/93	3.0	11.5	7.3	213	149	18.0	5.3	18.0	3.7	106	8.2	12.0	0.34	0.20	0.12	2.30	2.26	1%	88	71	0.35	0.31	
/13/93	3.3	11.5	7.3	241	158	20.0	8.8	17.0	3.8	105	11.0	13.0	4.54	0.20	0.12	2.40	2.34	2%	86	78	0.53	0.31	
/13/93	4.0	11.5	7.4	230	154	21.0	6.9	17.0	3.8	100	8.6	13.0		D.20	0.13		1		••	Ř1	0.48	0.31	
V13/93	3.6	12.0	7.2	234	166	19.0	6.5	17.0	3.8		8.3	12.0		0.20	0.11				92	74	0.47	0.31	
11/84	2.8	11.5	7.2	219	152	18.0	6.2	16.0	4.1	102	7.5	12.0		0.20	0.11	2.21	2.15	3%	83	70	0.3	0.28	
12/94	3.0	11.0	6.8	216	148	18.0	8.1	18.0	3.7	105	6.3	12.0		0.20	0.12	2.19	2.23	2%	87	70	0.36	0.28	
12/94	4.1	11.0	7.1	221	132	18.0	6.1	16.0	4.1	109	7.4	11.0		0.20	0.13	2.20	2.25	2%	88	70	0.25	0.28	
18/95	3.0	10.0	7.1	224	152	18.0	6.1	17.0	3.6	104	8.3	11.0		0.20	0.12	2.23	2.18	2%	85	70	0.32	0.34	
18/95	3.3	11.0	7.1	236	168	19.0	8.4	17.0	3.8	112	10.0	10.0		0.20	D.12	2.32	2.35	1%	91	74	0.43	0.34	
/11/95	4.0	11.0	7.1	237	158	20.0	8.7	17.0	3.9	115	8.7	11.0		0.20	0.12	2.30	2.38	0%	94	78	0.62	0.31	
11100	0	11.0	7.1	231	130	20.0	4.7	.7.0	0.0		0.7	. 1.0		U.20	12		2.30	- ~				0.	
of Data	28	28	28	28	28	28	28	28	28	17	28	28	3	27	28				22	28	28	27	
inimum	2.6	10.0	6.9	166	105	18.0	5.2	13.0	3.0	93	5.2	6.0	0.26	0.10	0.09				73	81	0.25	0.25	
aximum	4.1	13.0	7.7	241	168	21.0	6.9	18.0	4.1	115	11.0	13.0	0.68	0.40	0.13				94	81	0.70	0.34	
verage	3.2	11.3	7.3	205	145	17.4	5.0	15.4	3.6	102	7.5	11.6	0.43	0.20	0.11				82	68	0.41	0.30	- 2
d. Dev.	0.4	0.5	0.2	20	15	1.4	0.5	1.4	0.3	7	1.5	1,3	0.22	0.06	0.01				6	8	0.13	0.02	- 3



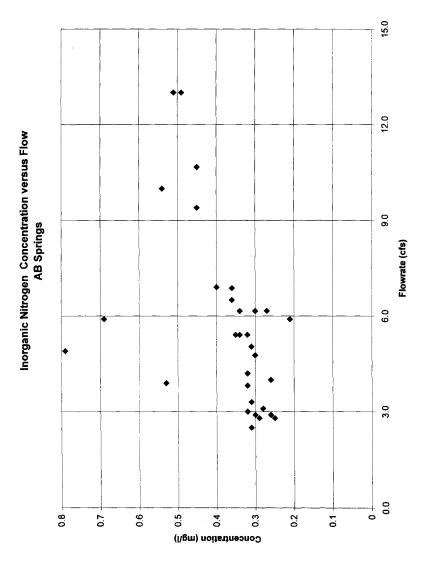
JGATENC:MAMMOTHWQWatql - AB TvsF 9/24/96

15.0 12.0 Total Dissolved Solid Concentration versus Flow AB Springs 9.0 Flowrate (cfs) 6.0 3.0 0.0 8 240 220 200 180 160 140 120 Concentration (mg/l)

JGATENC:MAMMOTHWQWatqi - AB TDSvsF 9/24/96

15.0 ** 12.0 Total Hardness versus Flow AB Springs • 9.0 Flowrate (cfs) 0.9 **‡** 3.0 0.0 901 32 8 92 8 22 29 82 8 22 2 Total Hardness (mg/l as CaCO3)

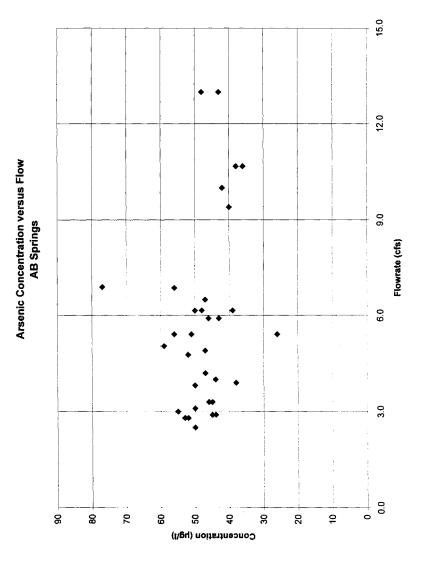
JGATENC:WAMMOTHWQWatqi - AB Hard vsF 9/24/96



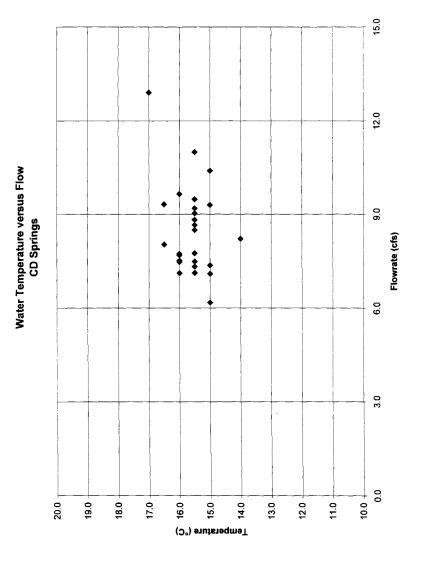
JGATENC: MAMMOTHIWQWatqi - AB NvsF 9/24/96

15.0 12.0 Ortho Phosphate Concentration versus Flow AB Springs 9.0 Flowrate (cfs) 6.0 3.0 0.0 Concentration (mg/l) 0.45 0.2 0.25 9.0 0.55 0.5 0.3

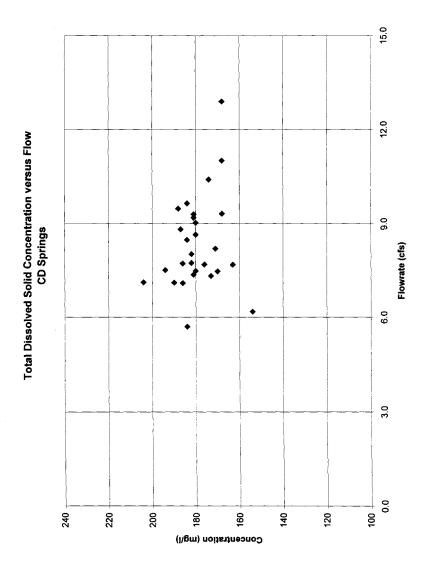
JGATENC:\MAMMOTH\WQ\Watqi - AB PvsF 9/24/96



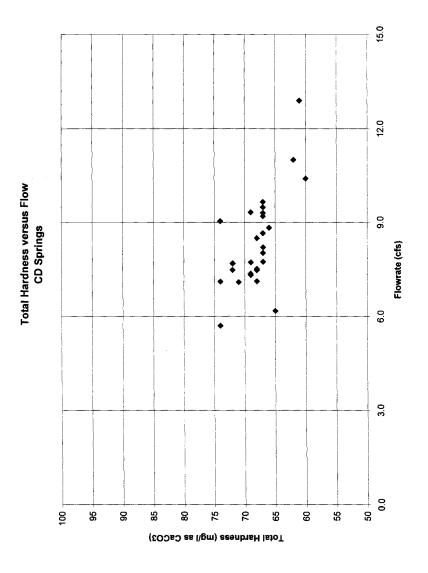
JGATENC:MAMMOTHWQWatqi - AB As vsF 9/24/96



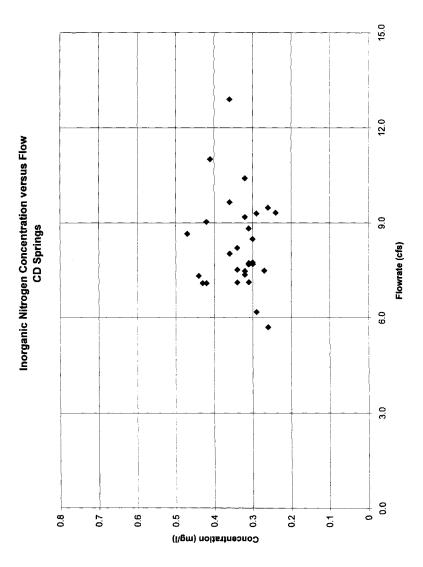
JGATENC:\MAMMOTH\WQ\Watq| - CD TvsF 9/24/96



JGATENC:MAMMOTHWQWatql - CD TDSvsF 9/24/96



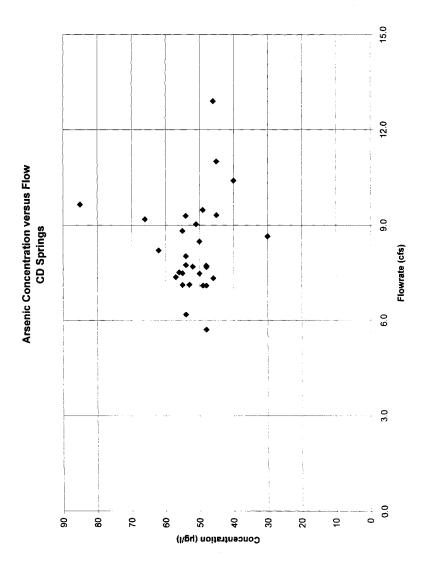
JGATENC:\MAMMOTH\WQ\Watql - CD Hard vsF 9/24/96



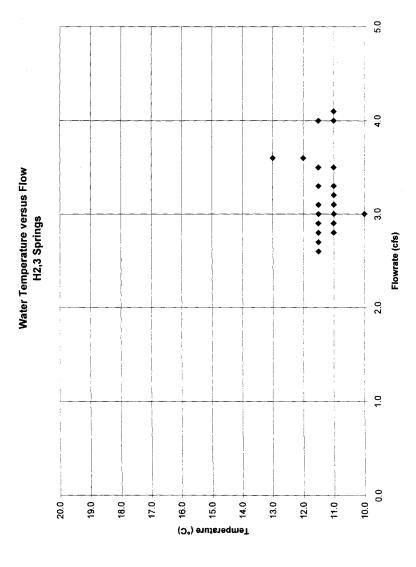
JGATENC:MAMMOTHWQWatql - CD NvsF 9/24/96

15.0 12.0 Ortho Phosphate Concentration versus Flow CD Springs 9.0 Flowrate (cfs) ***** 6.0 3.0 0.0 0.2 Concentration (mg/l) 0.45 0.00 0.35 9.0 0.55 0.5 0.25 0.3

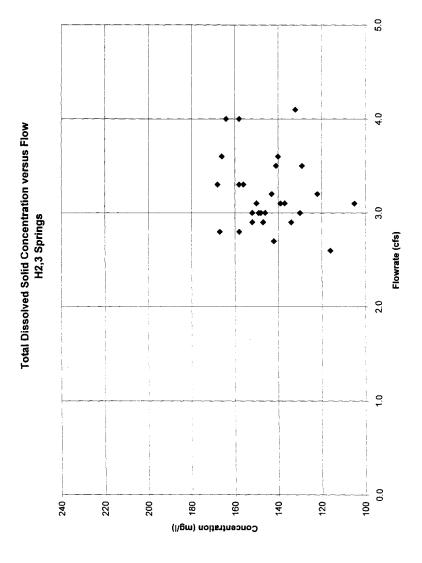
JGATENC:\MAMMOTH\WQ\Watql - CD PvsF 9/24/96



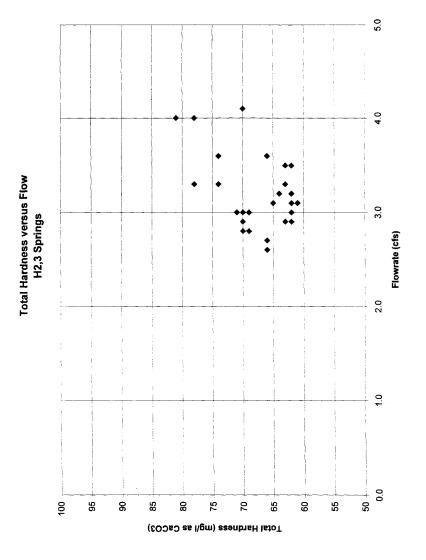
JGATENC:MAMMOTHWQWatqi - CD As vsF 9/24/96



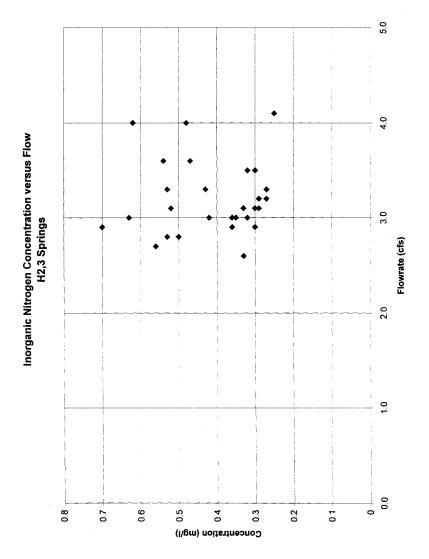
JGATENC:WAMMOTHNWQNVatqi - H23 TvsF 9/24/96



JGATENC:\MAMMOTH\WQ\Watqi - H23 TDSvsF 9/24/96



JGATENC:MAMMOTHWQWatqi - H23 Hard vsF 9/24/96



JGATENC:\MAMMOTH\WQ\Watq\ - H23 NvsF 9/24/96

JGATENC:MAMMOTHWQNWatql - H23 PvsF 9/24/96

5.0 4.0 Arsenic Concentration versus Flow H2,3 Springs • 3.0 Flowrate (cfs) 5.0 1.0 0.0 20 45 6 32 Concentration (µg/l) 15 5

JGATENC:MAMMOTHWQWatqi - H23 As vsF 9/24/96